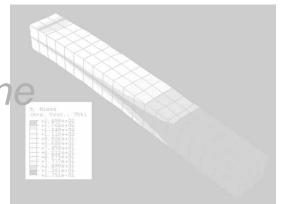
ARCHITECTURAL STRUCTURES I:

STATICS AND STRENGTH OF MATERIALS

DR. ANNE NICHOLS

SPRING 2008

lecture



beams:

deflection & design

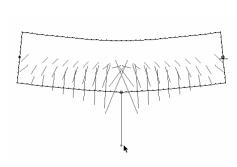
Lecture 21

**ENDS 231** 

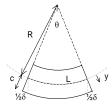
S2008abn

### Beam Deformations

- · curvature relates to
  - bending moment
  - modulus of elasticity
  - moment of inertia



M



$$curvature = \frac{M(x)}{EI}$$

$$\theta = slope = \int \frac{M(x)}{EI} dx$$

$$\Delta = deflection = \int \int \frac{M(x)}{EI} dx$$

Beam Deflection & Design 5 Architectural Structures I Lecture 21 **ENDS 231** 

# Design for Strength +...

- strength design
  - forces & material
- serviceability
  - limit deflection and cracking
  - control noise & vibration
  - no excessive settlement of foundations
  - durability
  - appearance
  - component damage
  - ponding



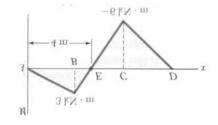
S2004abr

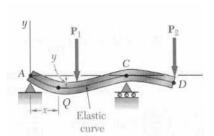
Beam Deflection & Design 4

Architectural Structures I **ENDS 231** 

# Deflected Shape & M(x)

- -M(x) gives shape indication
- boundary conditions must be met





Beam Deflection & Design 6 Lecture 21

Architectural Structures I ENDS 231

\$2004ahr

# **Boundary Conditions**

at pins, rollers, fixed supports: y = 0

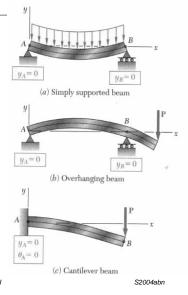
• at fixed supports:  $\theta = 0$ 

 at inflection points from symmetry:  $\theta = 0$ 

• 
$$y_{max}$$
 at  $\frac{dy}{dx} = 0$ 

Beam Deflection & Design 7 Lecture 21

Architectural Structures I ENDS 231



S2004abn

## Superpositioning

- if w can be superpositioned
  - $-\theta$  & y can
  - elastic range only!



Beam Deflection & Design 8 Lecture 21

Architectural Structures I ENDS 231

S2004abn

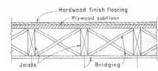
### **Deflection Limits**

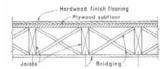
based on service condition, severity

Use	LL only	DL+LL
Roof beams:		
Industrial	L/180	L/120
Commercial		
plaster ceiling	L/240	L/180
no plaster	L/360	L/240
Floor beams:		
Ordinary Usage	L/360	L/240
Roof or floor (damageable elements)		L/480

# Lateral Buckling

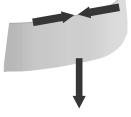
- lateral buckling caused by compressive forces at top coupled with insufficient rigidity
- can occur at low stress levels
- stiffen, brace or bigger I<sub>v</sub>





Beam Deflection & Design 10

Architectural Structures I ENDS 231

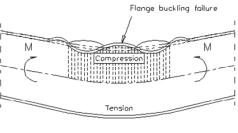


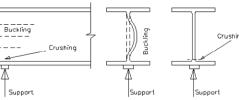
S2004abn

# Local Buckling

- steel I beams
- flange
  - buckle in direction of smaller radius of gyration
- web
  - force
  - "crippling"

Beam Deflection & Design 11





Architectural Structures I ENDS 231

S2004abn

S2004abn

# Local Buckling

# • flange

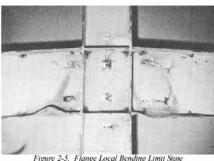


Figure 2-5. Flange Local Bending Limit State (Beedle, L.S., Christopher, R., 1964)

#### web



Beam Deflection & Design 15

Architectural Structures I ENDS 231

Su2004abn

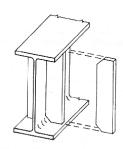
### Shear in Web

• panels in plate girders or webs with large shear

Architectural Structures I

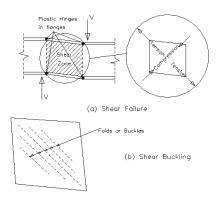
ENDS 231

- buckling in compression direction
- add stiffeners



stiffeners to prevent lateral buckling

Beam Deflection & Design 12 Lecture 21



### Shear in Web

· plate girders and stiffeners



Beam Deflection & Design 17

ENDS 231

Su2004abn

# Beam Design

- 1. Know  $F_{all}$  for the material or  $F_{ll}$  for LRFD
- 2. Draw V & M, finding M<sub>max</sub>



3. Calculate  $S_{reg'd}$   $(f_b \le F_b)$ 

D

4. Determine section size

$$S = \frac{bh^2}{6}$$

Beam Deflection & Design 13 Lecture 21 Architectural Structures I ENDS 231 S2004abn

# Beam Design

6. Evaluate shear stresses - horizontal  $(f_v \le F_v)$ 

• W and rectangles  $f_{v-\text{max}} = \frac{3V}{2A} \approx \frac{V}{A_{web}}$ 

• thin walled sections  $f_{v-\max} = \frac{VQ}{Ih}$ 

### Beam Design

- $4^*$ . Include self weight for  $M_{max}$ 
  - and repeat 3 & 4 if necessary

5. Consider lateral stability

Unbraced roof trusses were blown down in 1999 at this project in Moscow, Idaho.

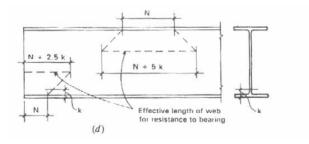
Photo: Ken Carper

Beam Deflection & Design 19 Lecture 18 Architectural Structures ENDS 231 Su2004abn

# Beam Design

7. Provide adequate bearing area at supports

 $f_p = \frac{P}{A} \le F_p$ 



# Beam Design

#### 8. Evaluate torsion

$$(f_v \leq F_v)$$

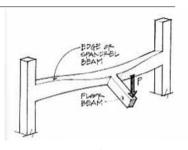
circular cross section

$$f_{v} = \frac{T\rho}{J}$$

ullet rectangular T

$$f_{v} = \frac{I}{c_1 a b^2}$$

Beam Deflection & Design 17 Lecture 18 Architectural Structures I ENDS 231



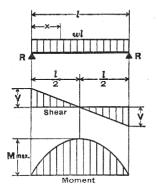
Rectangular Bars in Torsion			
a/b	c,	$c_2$	
1.0	° 0.208	0.1406	
1.2	0.219	0.1661	
1.5	0.231	0.1958	
2.0	0.246	0.229	
2.5	0.258	0.249	
3.0	0.267	0.263	
4.0	0.282	0.281	
5.0	0.291	0.291	
10.0	0.312	0.312	
$\infty$	0.333	0.333	

TABLE 3.1. Coefficients for

# Beam Design

### 9. - how to read charts

#### 1. SIMPLE BEAM-UNIFORMLY DISTRIBUTED LOAD



Beam Deflection & Design 18

Lecture 21

 $V_{X} \qquad = w \left($   $M \text{ max. (at center)} \qquad = \frac{wl^{2}}{8}$   $M_{X} \qquad = \frac{wx}{2}$ 

Architectural Structures I

ENDS 231

Total Equiv. Uniform Load . . . = wl

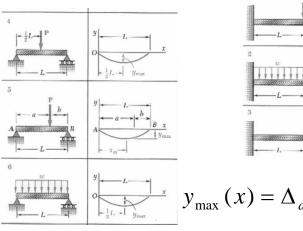
 $\Delta$ max. (at center) . . . =  $\frac{5 Wl^4}{384 EI}$ 

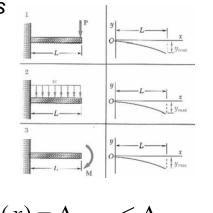
 $\Delta_{X}$  . . . . . . . . .  $=\frac{wX}{24EI}(I^{3}-2Ix^{2}+x^{3})$ 

S2004abn

# Beam Design

### 9. Evaluate deflections





 $y_{\text{max}}(x) = \Delta_{actual} \le \Delta_{allowable}$ 

Beam Deflection & Design 17 Lecture 21 Architectural Structures I ENDS 231 S2004abn