

*ARCHITECTURAL STRUCTURES I:
STATICS AND STRENGTH OF MATERIALS*

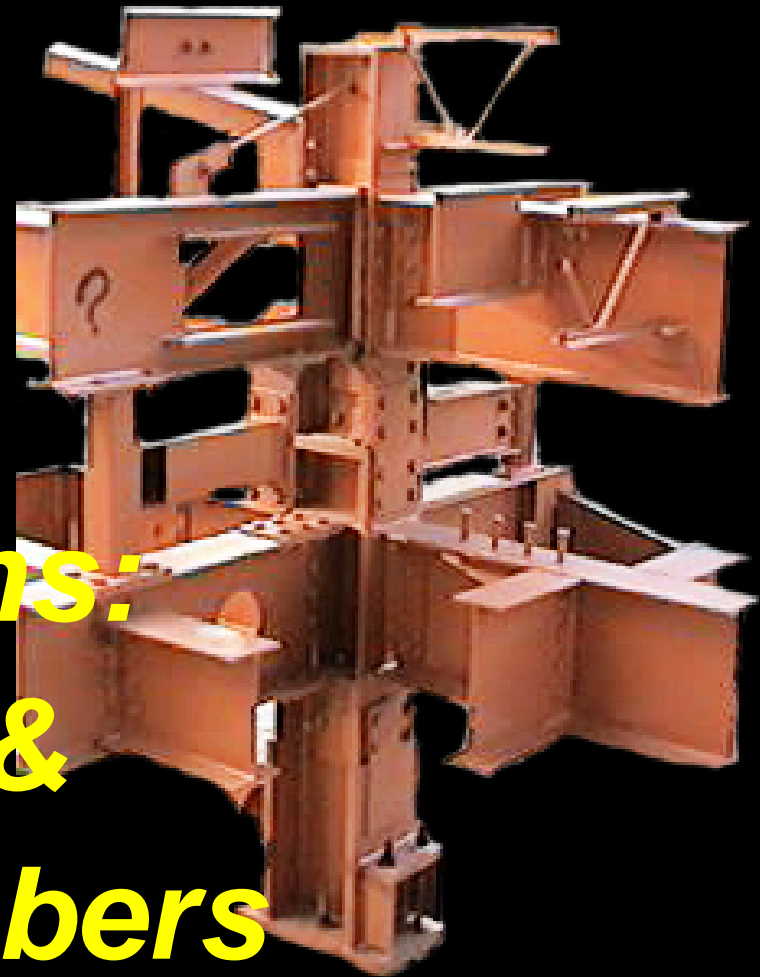
ENDS 231

DR. ANNE NICHOLS

FALL 2007

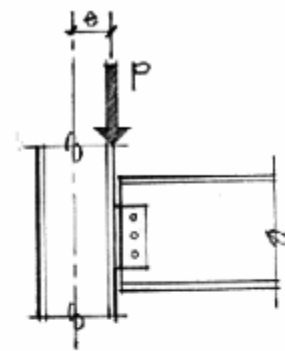
*lecture
twenty six*

***steel connections:
bolts, welds &
tension members***

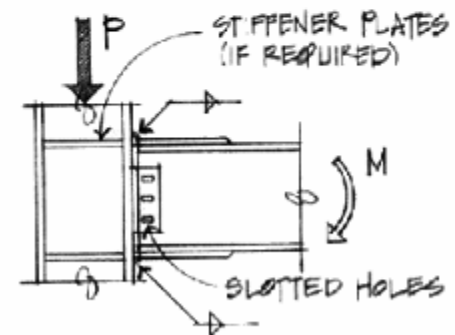


Connections

- *needed to:*
 - *support beams by columns*
 - *connect truss members*
 - *splice beams or columns*
- *transfer load*
- *subjected to*
 - *tension or compression*
 - *shear*
 - *bending*



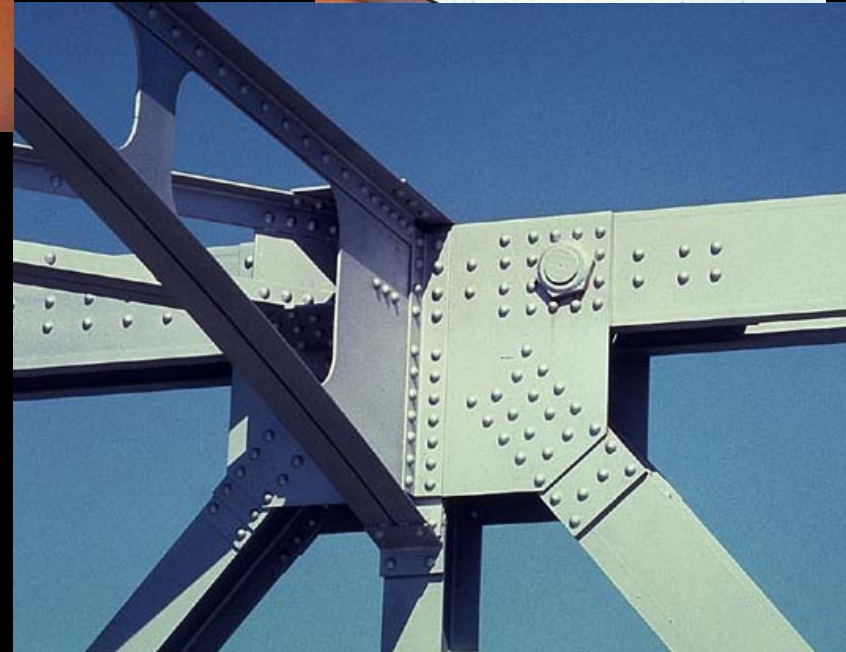
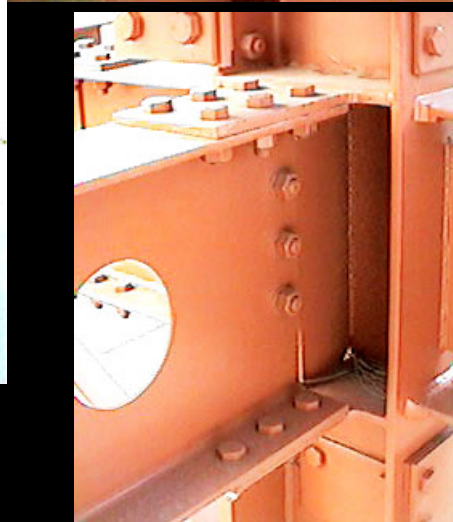
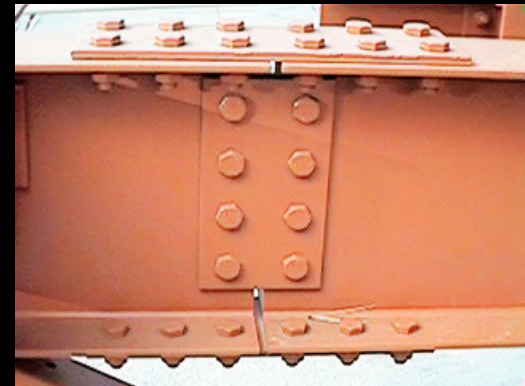
(a) Framed beam (shear) connection.
 $e = \text{Eccentricity}; M = P \times e$



(b) Moment connection (rigid frame).
 $M = \text{Moment due to beam bending}$

Bolts

- *bolted steel connections*



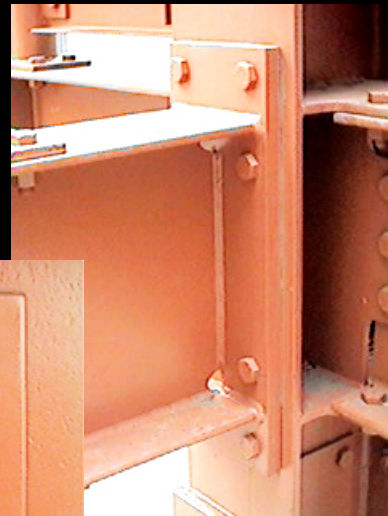
Connections 3
Lecture 26

Architectural Structures I
ENDS 231

F2007abn

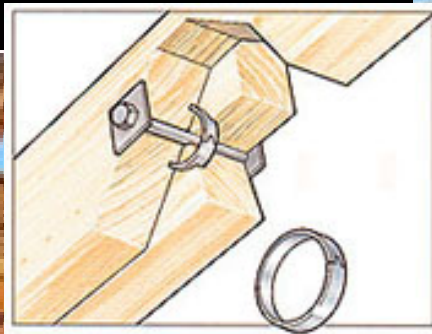
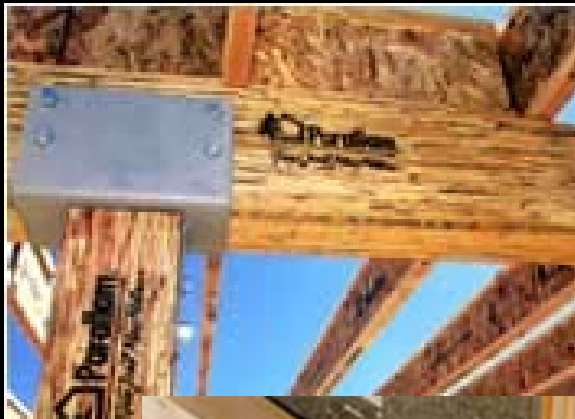
Welds

- *welded steel connections*



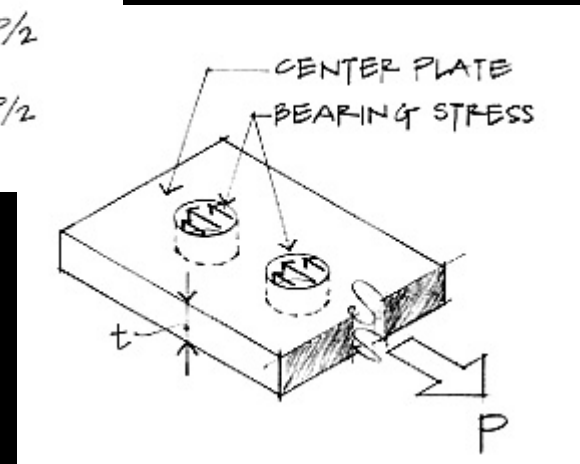
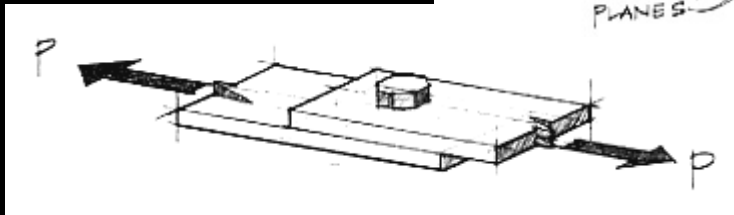
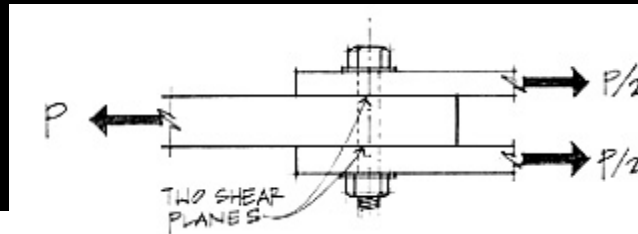
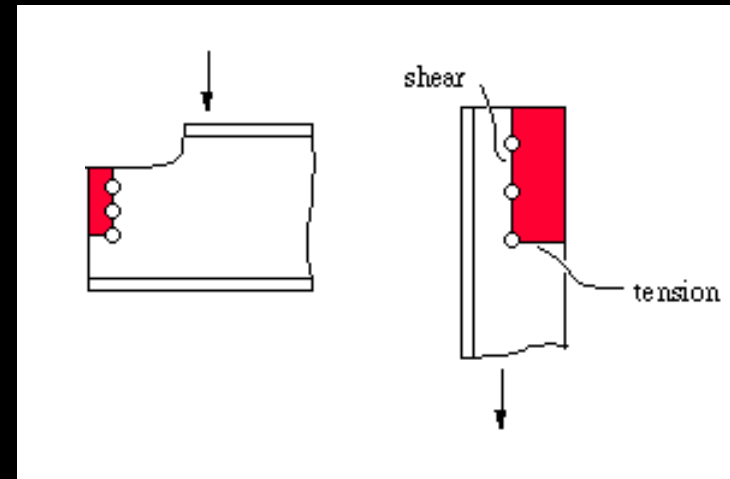
Fasteners

- *wood connections*



Bolted Connection Design

- *considerations*
 - *bearing stress*
 - *yielding*
 - *shear stress*
 - *single & double*
 - *member*
 - *rupture*



Bolted Connection Design

- ASD steel
 - shear:

$$f_v \leq F_v$$

- bolt strengths
- single & double
- bolt types
 - A325-SC, A490-SC
 - A325-N, A490-N
 - A325-X, A490-X

BOLTS, THREADED PARTS AND RIVETS
Shear
Allowable load in kips

		TABLE SHEAR											
ASTM Designation	Connection Type ^a	Hole Type ^b	F _v ksi	Loading ^c	Nominal Diameter d, in.								
					3/8	1/2	5/8	1	1 1/8	1 1/4	1 3/8	1 1/2	
					Area (Based on Nominal Diameter) in. ²								
					.3068	.4418	.6013	.7854	.9940	1.227	1.485	1.767	
Bolts	A307	STD NSL	10.0	S D	3.1	4.4	6.0	7.9	9.9	12.3	14.8	17.7	
					5.1	8.8	12.0	15.7	18.8	24.5	29.7	35.3	
	A325	SC ^d Class A	STD	17.0	S D	5.22	7.51	10.2	13.4	18.8	20.9	25.2	30.0
						10.4	15.0	20.4	26.7	33.8	41.7	50.5	60.1
						OVS, SSL	15.0	S D	4.60	6.63	9.02	11.8	14.9
		A325	LSL	12.0	S D	3.68	5.30	7.22	9.42	11.9	14.7	17.9	21.2
						7.36	10.6	14.4	18.8	23.9	29.4	35.6	42.4
						N	STD, NSL	21.0	S D	6.4	9.3	12.6	16.5
	A325	X	STD, NSL	30.0	S D	9.2	13.5	18.0	23.6	29.8	36.8	44.5	53.0
						18.4	26.5	36.1	47.1	58.8	73.6	89.1	106.0
	A490	SC ^d Class A	STD	21.0	S D	6.44	9.28	12.6	16.5	20.9	25.8	31.2	37.1
						12.9	18.6	25.3	33.0	41.7	51.5	62.4	74.2
						OVS, SSL	18.0	S D	5.52	7.95	10.8	14.1	17.9
		A490	LSL	15.0	S D	4.80	6.83	9.02	11.8	14.9	18.4	22.3	26.5
						9.20	13.0	18.0	23.6	29.8	36.8	44.6	53.0
						N	STD, NSL	28.0	S D	8.6	12.4	16.8	22.0
	A490	X	STD, NSL	40.0	S D	12.3	17.7	24.1	31.4	38.8	48.1	58.4	70.7
						24.5	35.3	48.1	62.8	79.6	98.2	119.0	141.0
Rivets	A502-1	STD	17.5	S D	5.4	7.7	10.5	13.7	17.4	21.5	26.0	30.8	
	A502-2	STD	22.0	S D	6.7	9.7	13.2	17.3	21.9	27.0	32.7	38.9	
	A502-3				13.5	19.4	26.5	34.6	43.7	54.0	65.3	77.7	
A36 (F _v =58 ksi)	N	STD	9.9	S D	3.0	4.4	6.0	7.8	9.8	12.1	14.7	17.5	
					6.1	8.7	11.9	15.6	19.7	24.3	29.4	35.0	
A36 (F _v =58 ksi)	X	STD	12.8	S D	3.9	5.7	7.7	10.1	12.7	15.7	19.0	22.6	

Bolted Connection Design

- *ASD steel*
 - *bearing:*
 - *bolts rarely fail by bearing*
 - *other part fails first*

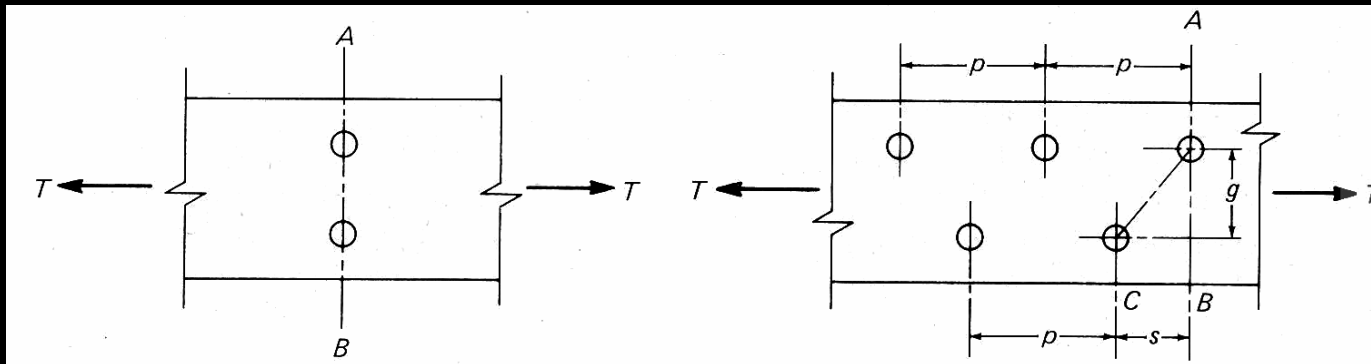
BOLTS AND THREADED PARTS
Bearing
Allowable loads in kips

TABLE BEARING
Slip-critical and Bearing-type Connections

Material Thickness	$F_u = 58$ ksi Bolt dia.			$F_u = 65$ ksi Bolt dia.			$F_u = 70$ ksi Bolt dia.			$F_u = 100$ ksi Bolt dia.		
	3/4	7/8	1	3/4	7/8	1	3/4	7/8	1	3/4	7/8	1
1/8	6.5	7.6	8.7	7.3	8.5	9.8	7.9	9.2	10.5	11.3	13.1	15.0
3/16	9.8	11.4	13.1	11.0	12.8	14.6	11.8	13.8	15.8	16.9	19.7	22.5
1/4	13.1	15.2	17.4	14.6	17.1	19.5	15.8	18.4	21.0	22.5	26.3	30.0
3/16	16.3	19.0	21.8	18.3	21.3	24.4	19.7	23.0	26.3	28.1	32.8	37.5
3/8	19.6	22.8	26.1	21.9	25.6	29.3	23.6	27.6	31.5	33.8	39.4	45.0
7/16	22.8	26.6	30.5	25.6	29.9	34.1	27.6	32.2	36.8		45.9	52.5
1/2	26.1	30.5	34.8	29.3	34.1	39.0	31.5	36.8	42.0			60.0
9/16	29.4	34.3	39.2	32.9	38.4	43.9		41.3	47.3			
5/8	32.6	38.1	43.5		42.7	48.8		45.9	52.5			
11/16		41.9	47.9		46.9	53.8			57.8			
3/4		45.7	52.2			58.5						
13/16			55.6									
7/8			60.9									
15/16												
1	52.2	60.9	69.6	58.5	68.3	78.0	63.0	73.5	84.0	90.0	105.0	120.0

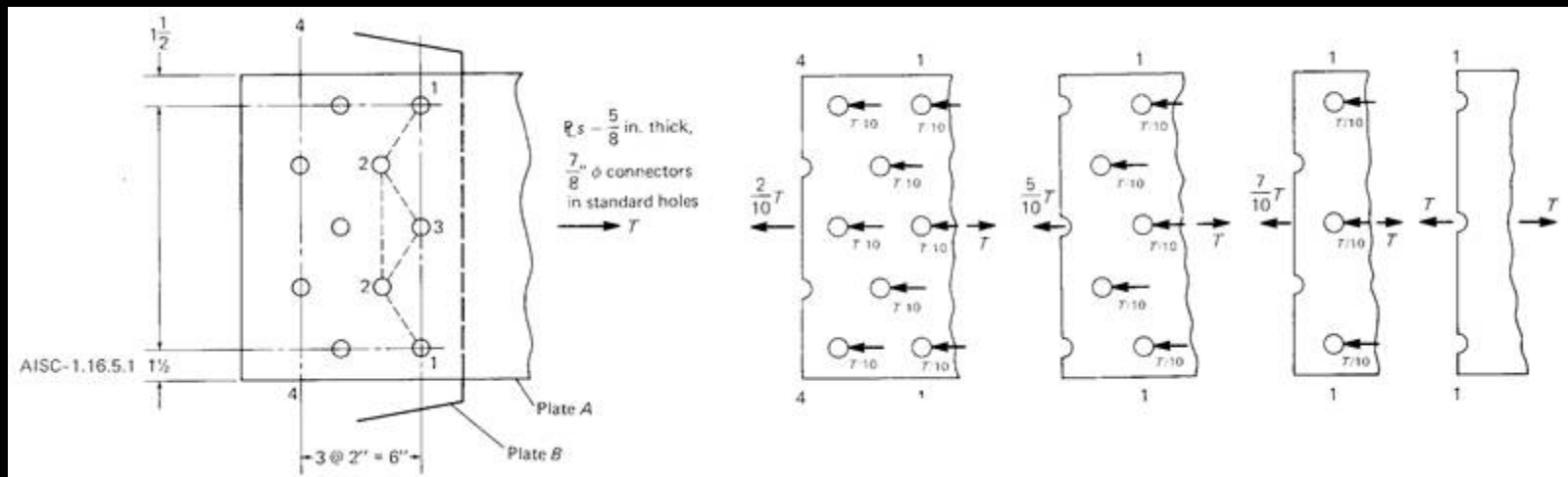
Tension Members

- steel members can have holes
- reduced area
- increased stress



Effective Net Area

- likely path to “rip” across
- bolts divide transferred force too



ASD – Tension Members

- non-pin connected members:
 - $F_t = 0.60F_y$ on gross area
 - $F_t = 0.50F_u$ on net area
- pin connected members:
 - $F_t = 0.45F_y$ on net area
- threaded rods of approved steel:
 - $F_t = 0.33F_u$ on major diameter
 - (for static loading only)



LRFD - Tension Members

- *limit states for failure* $P_u \leq \phi_t P_n$

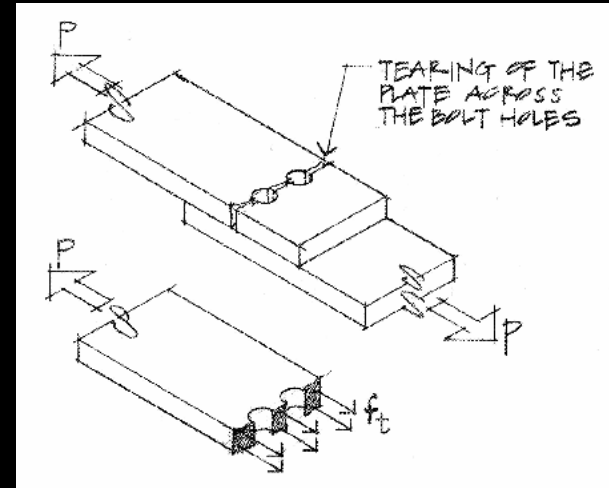
1. *yielding* $\phi_t = 0.9$ $P_n = F_y A_g$

2. *rupture** $\phi_t = 0.75$ $P_n = F_u A_e$

A_g - gross area

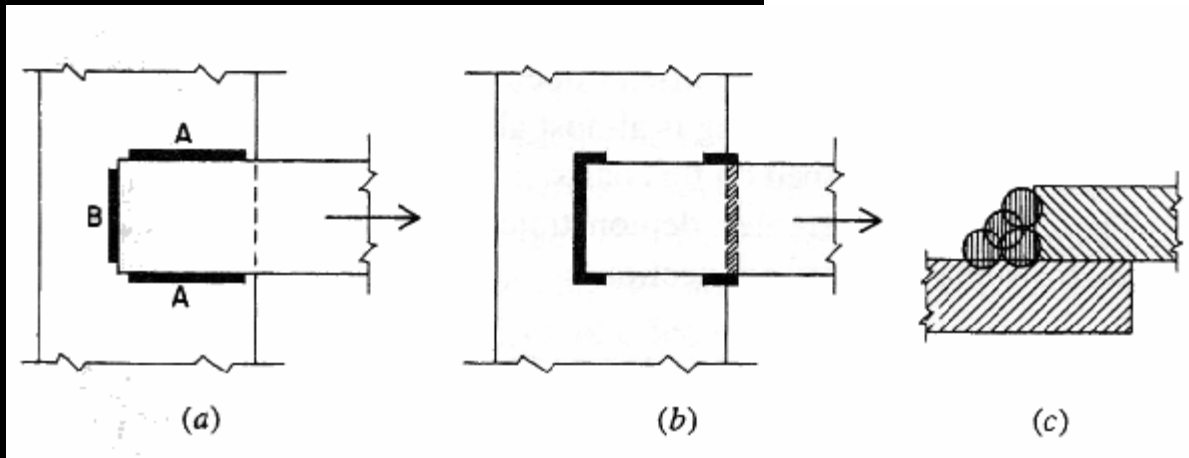
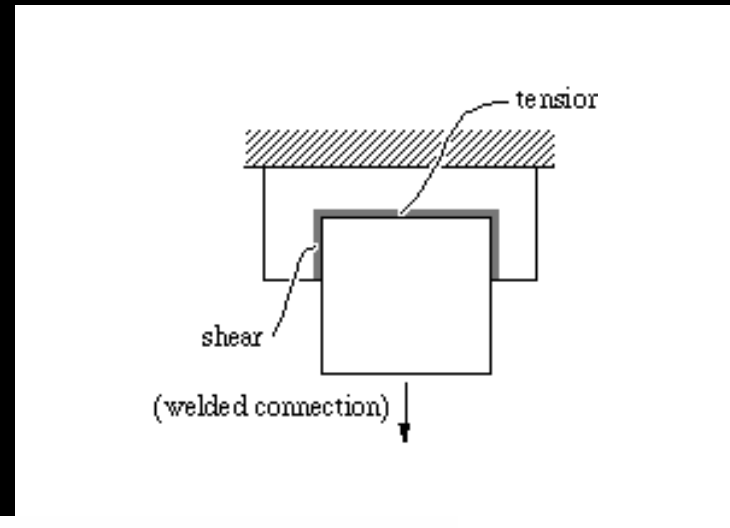
A_e - effective net area

F_u - tensile strength
of the steel (ultimate)



Welded Connection Design

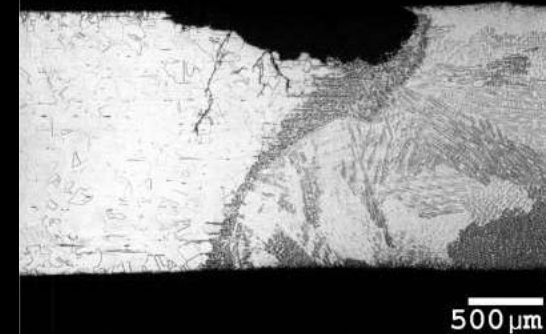
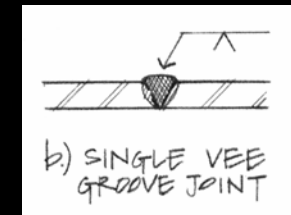
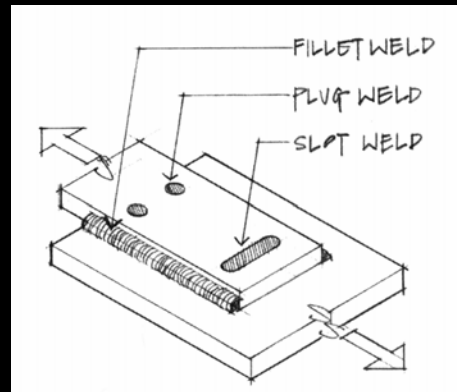
- *considerations*
 - *shear stress*
 - *yielding*
 - *rupture*



Welded Connection Design

- weld terms

- butt weld
- fillet weld
- plug weld
- throat



- weld materials

- E60XX
- E70XX
- $F_{EXX} = 70 \text{ ksi}$

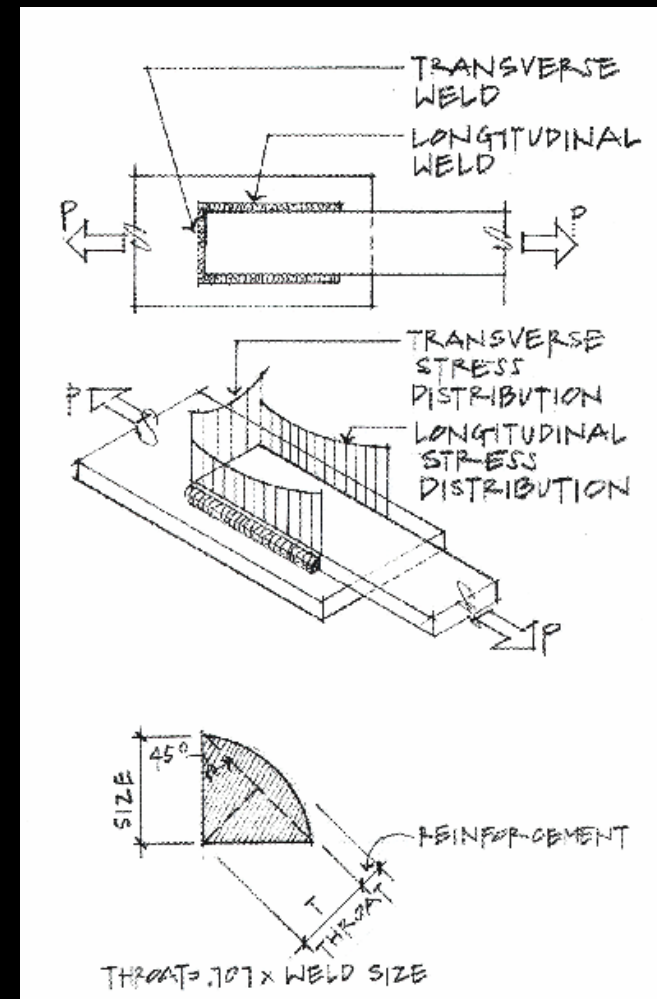
TABLE J2.4
Minimum Size of Fillet Welds

Material Thickness of Thicker Part Joined, in. (mm)	Minimum Size of Fillet Weld[a] in. (mm)
To 1/4 (6) inclusive	1/8 (3)
Over 1/4 (6) to 1/2 (13)	3/16 (5)
Over 1/2 (13) to 3/4 (19)	1/4 (6)
Over 3/4 (19)	5/16 (8)

[a] Leg dimension of fillet welds. Single pass welds must be used.
[b] See Section J2.20 for maximum size of fillet welds.

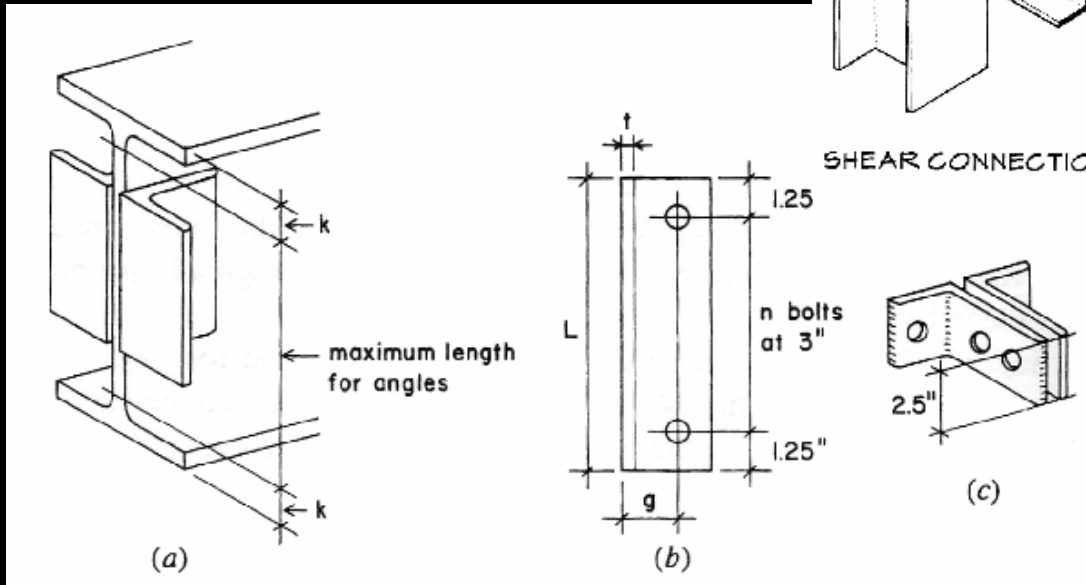
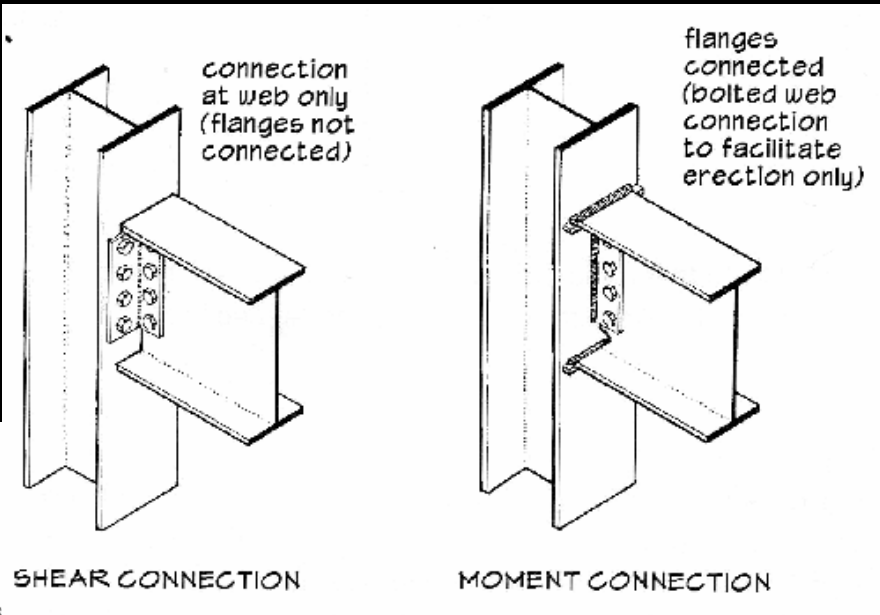
Welded Connection Design

- ASD
 - shear $f_v \leq F_v$
 - $F_v = 0.30F_{weld}$
 - throat
 - $T = 0.707 \times \text{weld size}$
 - area
 - $A = T \times \text{length of weld}$
 - weld metal generally stronger than base metal (ex. $F_y = 50 \text{ ksi}$)



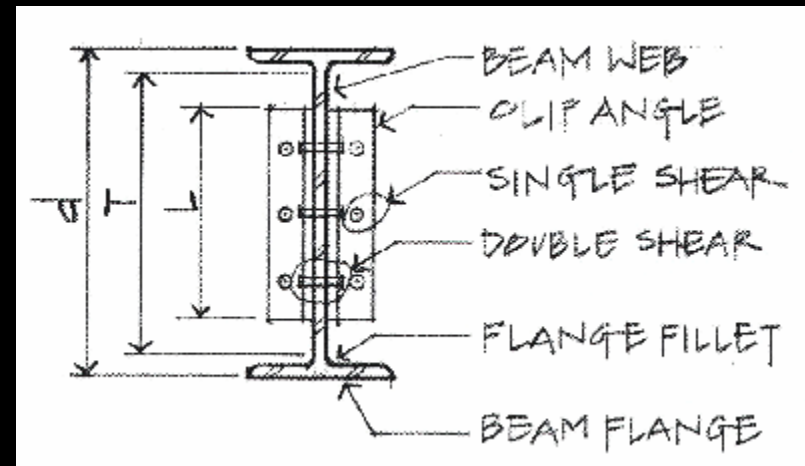
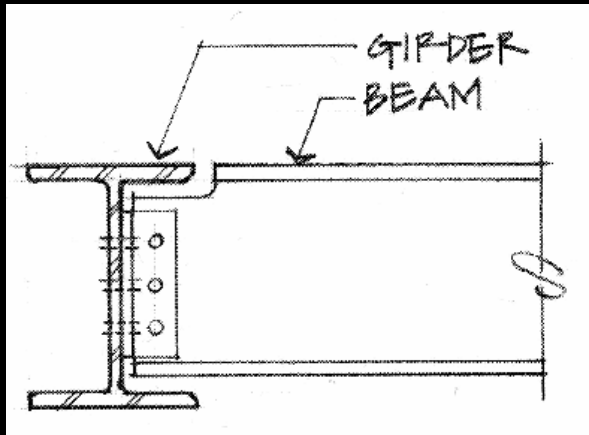
Framed Beam Connections

- *angles*
 - *bolted*
 - *welded*



Framed Beam Connections

- *terms*
 - *coping*

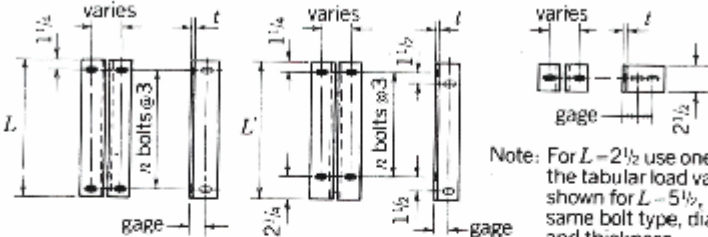


Framed Beam Connections

- tables for standard bolt holes & spacings
- $n = \# \text{ bolts}$
- angle leg thickness
- length needed

FRAMED BEAM CONNECTIONS
Bolted

TABLE Allowable loads in kips



STAGGERED BOLT
ALTERNATE

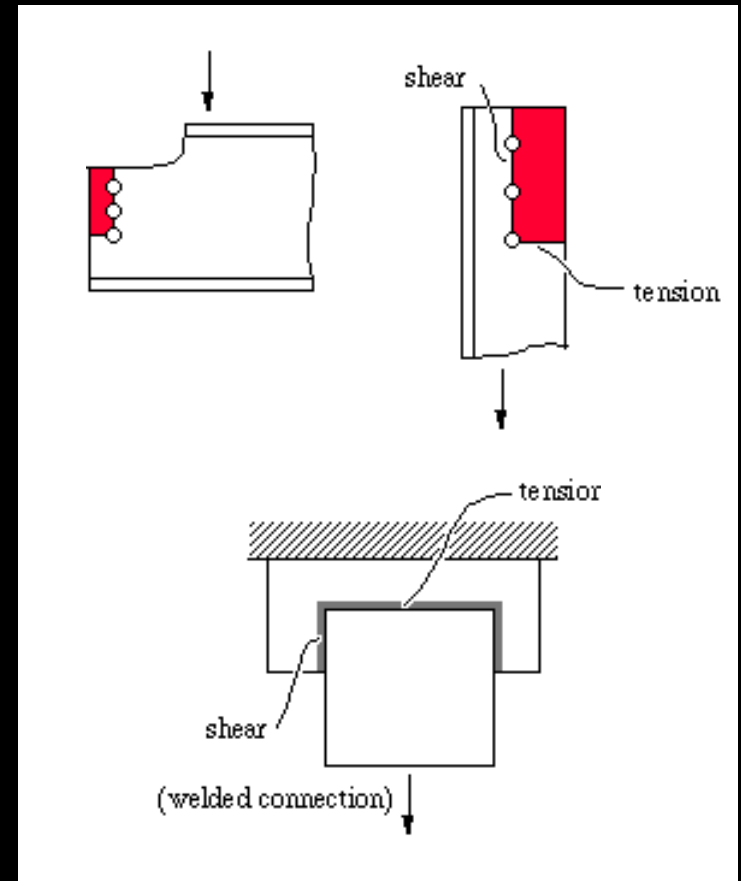
Note: For $L = 2\frac{1}{2}$ use one half the tabular load value shown for $L = 5\frac{1}{2}$, for the same bolt type, diameter, and thickness.

TABLE Bolt Shear^a
For bolts in **bearing-type** connections with standard or slotted holes.

Bolt Type		A325-N			A490-N			A325-X			A490-X			
F_u , Ksi		21.0			28.0			30.0			40.0			
Bolt Dia., d In.		$\frac{3}{4}$	$\frac{7}{8}$	1	$\frac{3}{4}$	$\frac{7}{8}$	1	$\frac{3}{4}$	$\frac{7}{8}$	1	$\frac{3}{4}$	$\frac{7}{8}$	1	
Angle Thickness t , In.		$\frac{3}{16}$	$\frac{3}{8}$	$\frac{9}{16}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{3}{8}$	$\frac{5}{8}$	$\frac{5}{8}$	$\frac{1}{2}$	$\frac{5}{8}$	$\frac{5}{8}$	
L In.	L' In.													
	n													
29½	31	10	186	253	330	247	337	440 ^b	285	361	^c	353	481	^c
26½	28	9	167	227	297	223	303	396 ^b	239	325	^c	318	433	^c
23½	25	8	148	202	264	198	269	352 ^b	212	289	^c	283	385	^c
20½	22	7	130	177	231	173	236	308 ^b	186	253	^c	247	337	^c
17½	19	6	111	152	198	148	202	264 ^b	159	216	283	212	289	377
14½	16	5	92.8	128	185	124	168	220 ^b	133	180	236	177	242	314
11½	13	4	74.2	101	132	99.0	135	176 ^b	106	144	188	141	192	251

Beam Connections

- *LRFD provisions*
 - *shear yielding*
 - *shear rupture*
 - *block shear rupture*
 - *tension yielding*
 - *tension rupture*
 - *local web buckling*
 - *lateral torsional buckling*

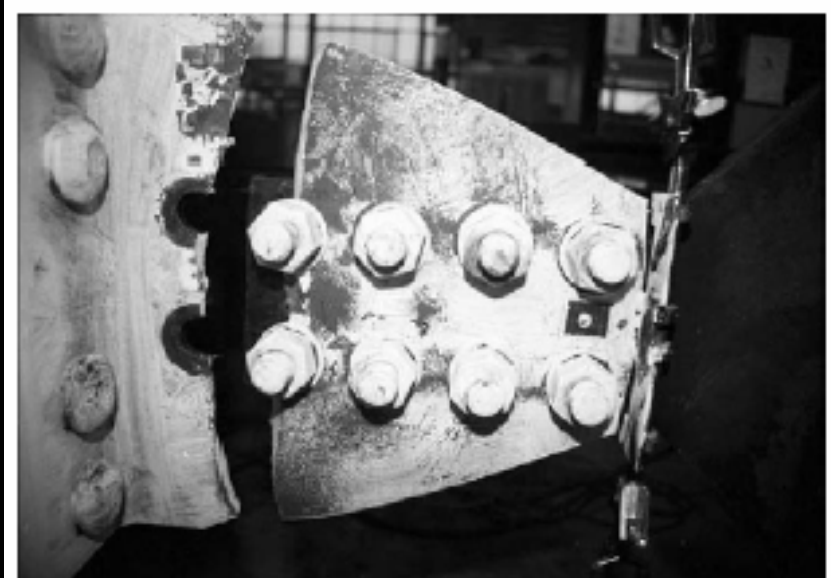


Beam Connections

- *block shear rupture*
- *tension rupture*



*Figure 2-1. Block Shear Rupture Limit State
(Photo by J.A. Swanson and R. Leon, courtesy of
Georgia Institute of Technology)*



*Figure 2-14. Tension Fracture Limit State
(Photo by J.A. Swanson and R. Leon,
courtesy of Georgia Institute of Technology)*