

**ARCHITECTURAL STRUCTURES I:
STATICS AND STRENGTH OF MATERIALS**

ENDS 231

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FALL 2007

**lecture
twenty four**

column design



Design Methods

- *know*
 - *loads or lengths*
- *select*
 - *section or load*
 - *adequate for strength and no buckling*

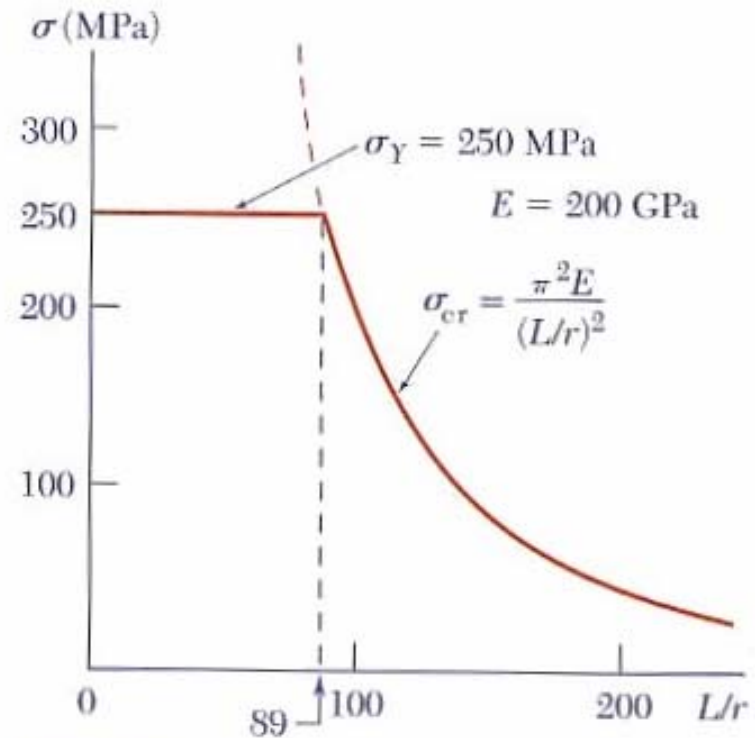


Fig. 10.9

Allowable Stress Design (ASD)

- AISC 9th ed

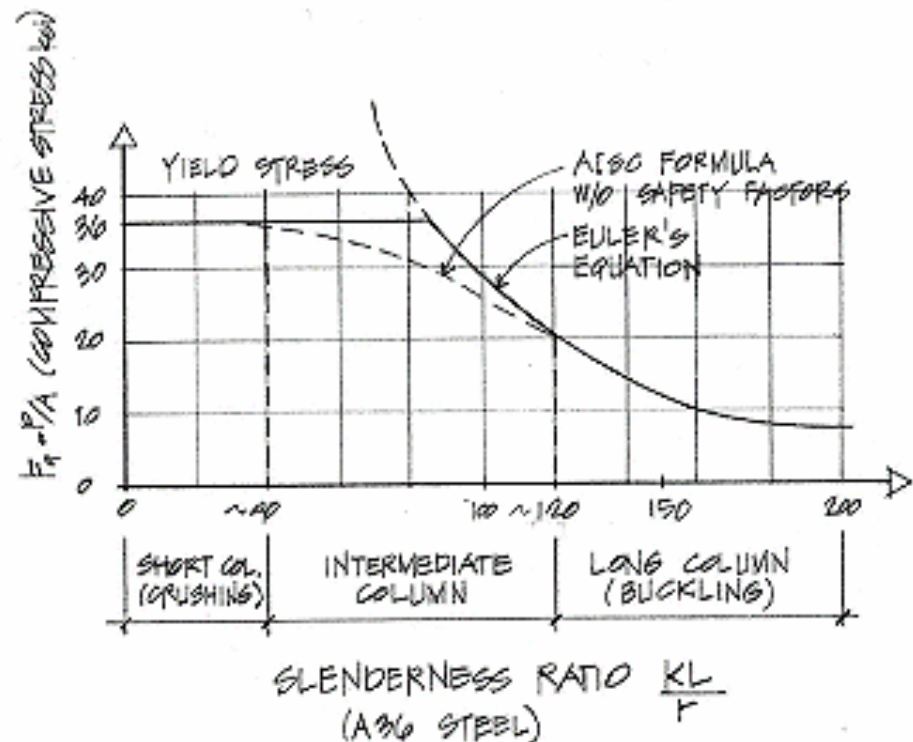
$$F_a = \frac{f_{critical}}{F.S.} = \frac{12\pi^2 E}{23 \left(\frac{Kl}{r} \right)^2}$$

- slenderness ratio $\frac{Kl}{r}$

– for $kl/r \geq C_c$ = 126.1 with $F_y = 36$ ksi
= 107.0 with $F_y = 50$ ksi

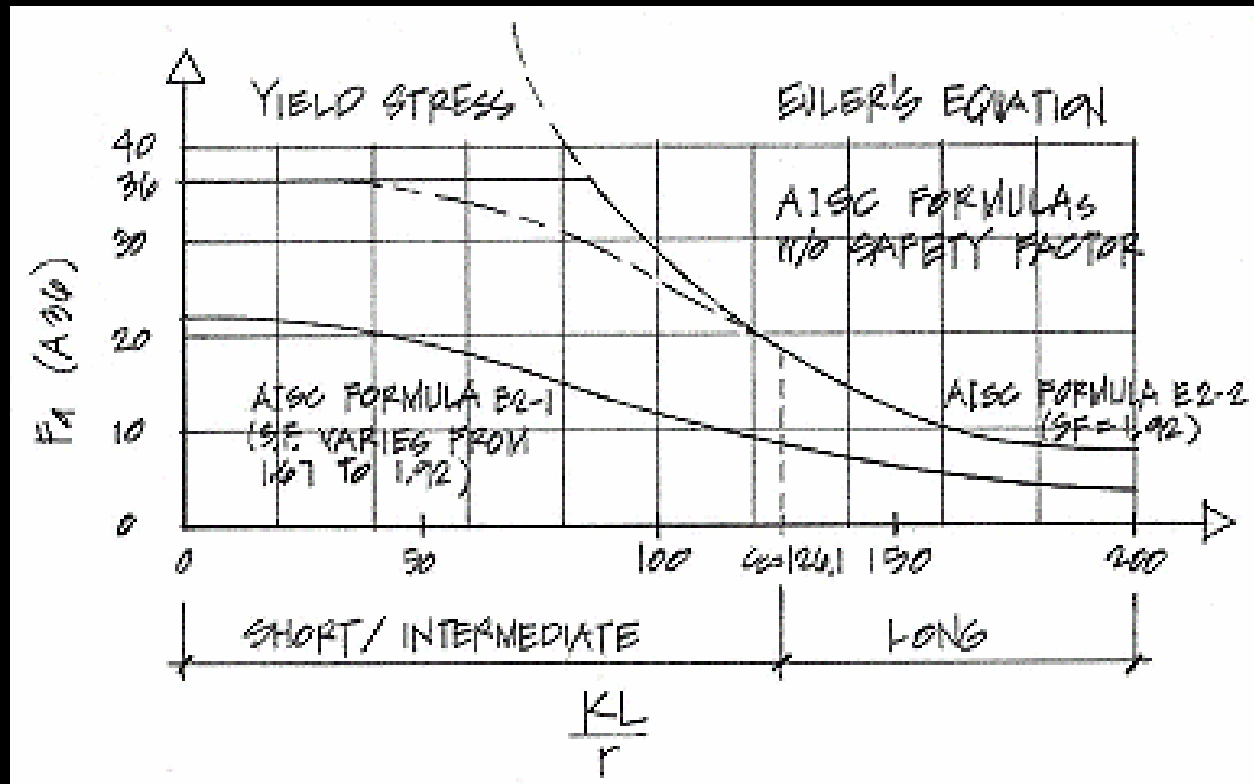
C_c and Euler's Formula

- $Kl/r < C_c$
 - short and stubby
 - parabolic transition
- $Kl/r > C_c$
 - Euler's relationship
 - < 200 preferred



$$C_c = \sqrt{\frac{2\pi^2 E}{F_y}}$$

C_c and Euler's Formula



Short / Intermediate

- $L_e/r < C_c$

$$F_a = \left[1 - \frac{\left(Kl/r \right)^2}{2C_c^2} \right] \frac{F_y}{F.S.}$$

– where

$$F.S. = \frac{5}{3} + \frac{3\left(Kl/r \right)}{8C_c} - \frac{\left(Kl/r \right)^3}{8C_c^3}$$

Procedure for Analysis

1. calculate KL/r

- biggest of KL/r with respect to x axes and y axis

2. find F_a from Table 10.1 or 10.2

- pp. 361 - 364

3. compute $P_{allowable} = F_a \cdot A$

- or find $f_{actual} = P/A$

4. is $P \leq P_{allowable}$? (or is $f_{actual} \leq F_a$?)

- yes: ok
- no: overstressed and no good

Procedure for Design

1. guess a size (pick a section)
2. calculate KL/r
 - biggest of KL/r with respect to x axes and y axis
3. find F_a from Table 10.1 or 10.2
 - pp. 361 - 364
4. compute $P_{allowable} = F_a \cdot A$
 - or find $f_{actual} = P/A$

Procedure for Design (cont'd)

5. *is $P \leq P_{allowable}$? (or is $f_{actual} \leq F_a$?)*

- *yes: ok*
- *no: pick a bigger section and **go back to step 2.***

6. *check design efficiency*

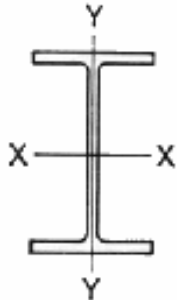
- *percentage of stress = $\frac{P_{actual}}{P_{allowable}} \cdot 100\%$*
- *if between 90-100%: good*
- *if < 90%: pick a smaller section and **go back to step 2.***

Column Charts

Table C-50
Allowable Stress
For Compression Members of 50-ksi Specified Yield Stress Steel^a

$\frac{Kl}{r}$	F_a (ksi)	$\frac{Kl}{r}$	F_a (ksi)	$\frac{Kl}{r}$	F_a (ksi)	$\frac{Kl}{r}$	F_a (ksi)	$\frac{Kl}{r}$	F_a (ksi)
1	29.94	41	25.69	81	18.81	121	10.20	161	5.76
2	29.87	42	25.55	82	18.61	122	10.03	162	5.69
3	29.80	43	25.40	83	18.41	123	9.87	163	5.62
4	29.73	44	25.26	84	18.20	124	9.71	164	5.55
5	29.66	45	25.11	85	17.99	125	9.56	165	5.49
6	29.58	46	24.96	86	17.79	126	9.41	166	5.42
7	29.50	47	24.81	87	17.58	127	9.26	167	5.35
8	29.42	48	24.66	88	17.37	128	9.11	168	5.29
9	29.34	49	24.51	89	17.15	129	8.97	169	5.23
10	29.26	50	24.35	90	16.94	130	8.84	170	5.17
11	29.17	51	24.19	91	16.72	131	8.70	171	5.11
12	29.08	52	24.04	92	16.50	132	8.57	172	5.05
13	28.99	53	23.88	93	16.29	133	8.44	173	4.99
14	28.90	54	23.72	94	16.06	134	8.32	174	4.93
15	28.80	55	23.55	95	15.84	135	8.19	175	4.88
16	28.71	56	23.39	96	15.62	136	8.07	176	4.82
17	28.61	57	23.22	97	15.39	137	7.96	177	4.77

Column Charts



COLUMNS
W shapes

$F_y = 36$ ksi

$F_y = 50$ ksi

Allowable axial loads in kips

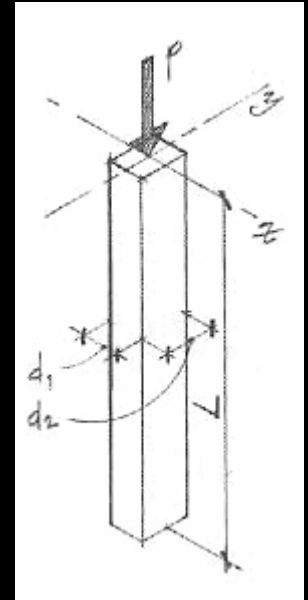
Designation		W8											
		67		58		48		40		35		31	
Wt./ft.													
F_y		36	50	36	50	36	50	36	50	36	50	36	50
Aspect to least radius of gyration r_y	0	426	591	369	513	305	423	253	351	222	309	197	274
	6	387	525	336	455	276	375	229	310	201	272	178	241
	7	379	510	328	442	270	363	223	300	197	264	174	234
	8	370	494	320	428	263	352	218	290	191	255	170	226
	9	360	477	312	413	256	339	212	279	186	246	165	217
	10	350	459	303	397	249	326	205	268	180	236	160	208
	11	339	440	293	380	241	312	199	256	174	225	154	199
	12	328	420	283	363	233	297	192	244	168	214	149	189
	13	316	399	273	344	224	282	184	231	162	202	143	179
	14	304	378	263	325	215	266	177	217	155	190	137	168
	15	292	355	251	305	206	249	169	203	148	177	131	156
	16	279	331	240	284	196	232	160	188	141	164	124	145
	17	265	307	228	263	186	214	152	172	133	150	117	132

Wood Columns

- *slenderness ratio* = $L/d_{min} = L/d_1$
 - d_1 = smaller dimension
 - $l_e/d \leq 50$ (max)

$$f_c = \frac{P}{A} \leq F'_c$$

- where F'_c is the allowable compressive strength parallel to the grain



Allowable Wood Stress

$$F'_c = F_c (C_D)(C_M)(C_t)(C_F)(C_p)$$

- where:

F_c = compressive strength
parallel to grain

C_D = load duration factor

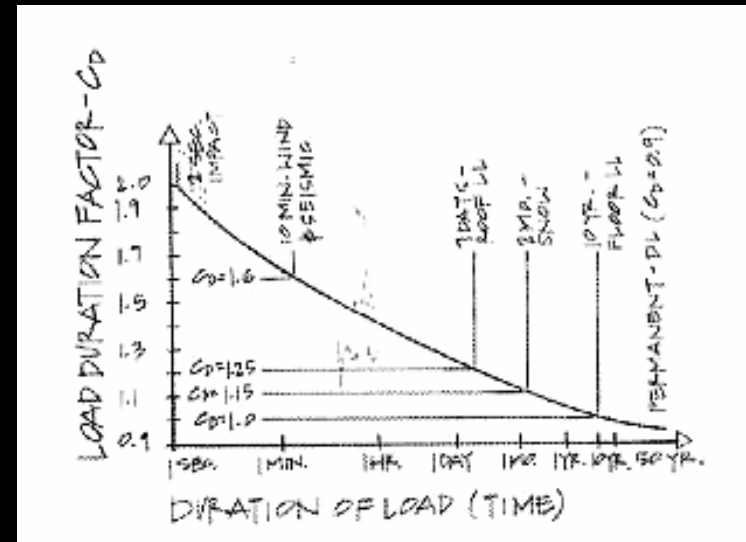
C_M = wet service factor
(1.0 dry)

C_t = temperature factor

C_F = size factor

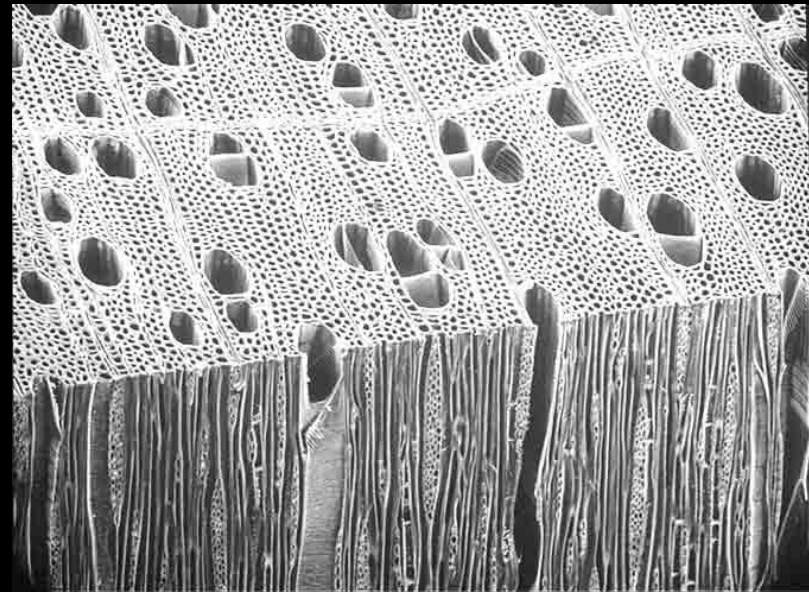
C_p = column stability factor

(Table 10.3)



Strength Factors

- *wood properties and load duration, C_D*
 - *short duration*
 - *higher loads*
 - *normal duration*
 - *> 10 years*



- *stability, C_p*
 - *combination curve - tables*

$$F'_c = F_c^* C_p = (F_c C_D) C_p$$

C_p Charts – Appendix A, Table 14

Column Stability Factor C_p

C_p			$F_c' = C_p \cdot F_c^*$			$F_{CE} = \frac{30 E}{(L/d)^2}$ for sawn posts			$F_{CE} = \frac{418 E}{(L/d)^2}$ for Glu-Lam posts		
$\frac{F_{CE}}{F_c'}$	Sawn C_p	Glu-Lam C_p	$\frac{F_{CE}}{F_c'}$	Sawn C_p	Glu-Lam C_p	$\frac{F_{CE}}{F_c'}$	Sawn C_p	Glu-Lam C_p	$\frac{F_{CE}}{F_c'}$	Sawn C_p	Glu-Lam C_p
0.00	0.000	0.000	0.60	0.500	0.598	1.20	0.750	0.822	2.40	0.894	0.940
0.01	0.010	0.010	0.61	0.506	0.545	1.22	0.755	0.826	2.45	0.897	0.941
0.02	0.020	0.020	0.62	0.512	0.552	1.24	0.760	0.831	2.50	0.899	0.943
0.03	0.030	0.030	0.63	0.518	0.559	1.26	0.764	0.836	2.55	0.901	0.944
0.04	0.040	0.040	0.64	0.524	0.566	1.28	0.769	0.840	2.60	0.904	0.946
0.05	0.049	0.050	0.65	0.530	0.573	1.30	0.773	0.844	2.65	0.906	0.947
0.06	0.059	0.060	0.66	0.536	0.580	1.32	0.777	0.848	2.70	0.908	0.949
0.07	0.069	0.069	0.67	0.542	0.587	1.34	0.781	0.852	2.75	0.910	0.950
0.08	0.079	0.079	0.68	0.548	0.593	1.36	0.785	0.855	2.80	0.912	0.951
0.09	0.088	0.089	0.69	0.553	0.600	1.38	0.789	0.859	2.85	0.914	0.952
0.10	0.098	0.099	0.70	0.559	0.607	1.40	0.793	0.862	2.90	0.916	0.953
0.11	0.107	0.109	0.71	0.564	0.613	1.42	0.796	0.865	2.95	0.917	0.954
0.12	0.117	0.118	0.72	0.569	0.619	1.44	0.800	0.868	3.00	0.919	0.955
0.13	0.126	0.128	0.73	0.575	0.626	1.46	0.803	0.871	3.05	0.920	0.956
0.14	0.136	0.138	0.74	0.580	0.632	1.48	0.807	0.874	3.10	0.922	0.957
0.15	0.145	0.147	0.75	0.585	0.638	1.50	0.810	0.877	3.15	0.923	0.958
0.16	0.154	0.157	0.76	0.590	0.644	1.52	0.813	0.879	3.20	0.925	0.959
0.17	0.164	0.167	0.77	0.595	0.650	1.54	0.816	0.882	3.25	0.926	0.960
0.18	0.173	0.176	0.78	0.600	0.655	1.56	0.819	0.884	3.30	0.927	0.961
0.19	0.182	0.186	0.79	0.605	0.661	1.58	0.822	0.887	3.35	0.929	0.961

Column Charts – Appendix A, 12 & 13

Table 12 Allowable Column Loads—Selected Species/Sizes. (Continued)

Eff.										8×8	A = 56.25	8×10	A = 71.25	8×12	A = 86.25
Col.	<i>l/d</i>	<i>(l/d)</i> sq	<i>F_{ce}</i>	<i>F_{ce}/F_c'</i>		<i>C_p</i>		<i>F_c</i> (psi)		<i>P_a</i> (k)		<i>P_a</i> (k)		<i>P_a</i>	
Len(ft)				Norm	Snow	Norm	Snow	Norm	Snow	Norm	Snow	Norm	Snow	Norm	Snow
12	19.2	368.64	1302.08	1.30	1.13	.7731	.7315	773	841	43.5	47.3	55.1	59.9	66.7	72.6
13	20.8	432.64	1109.47	1.11	0.96	.7258	.6767	726	778	40.8	43.8	51.7	55.4	62.6	67.1
14	22.4	501.76	956.63	0.96	0.83	.6767	.6235	677	717	38.1	40.3	48.2	51.1	58.4	61.8
15	24.00	576.00	833.33	0.83	0.72	.6235	.5694	624	655	35.1	36.8	44.4	46.7	53.8	56.5
16	25.60	655.36	732.42	0.73	0.64	.5747	.5244	575	603	32.3	33.9	40.9	43.0	49.6	52.0
17	27.20	739.84	648.79	0.65	0.56	.5303	.4744	530	546	29.8	30.7	37.8	38.9	45.7	47.1
18	28.80	829.44	578.70	0.58	0.50	.4873	.4336	487	499	27.4	28.0	34.7	35.5	42.0	43.0
19	30.40	924.16	519.39	0.52	0.45	.4475	.3975	448	457	25.2	25.7	31.9	32.6	38.6	39.4
20	32.00	1024.00	468.75	0.47	0.41	.4122	.3673	412	422	23.2	23.8	29.4	30.1	35.6	36.4
21	33.60	1128.96	425.17	0.43	0.37	.3826	.3360	383	386	21.5	21.7	27.3	27.5	33.0	33.3
22	35.20	1239.04	387.40	0.39	0.34	.3518	.3118	352	359	19.8	20.2	25.1	25.5	30.3	30.9
23	36.80	1354.24	354.44	0.35	0.31	.3199	.2869	320	330	18.0	18.6	22.8	23.5	27.6	28.5
24	38.40	1474.56	325.52	0.33	0.28	.3035	.2615	304	301	17.1	16.9	21.6	21.4	26.2	25.9
25	40.00	1600.00	300.00	0.30	0.26	.2785	.2442	279	281	15.7	15.8	19.8	20.0	24.0	24.2
26	41.60	1730.56	277.37	0.28	0.24	.2615	.2267	262	261	14.7	14.7	18.6	18.6	22.6	22.5
27	43.20	1866.24	257.20	0.26	0.22	.2442	.2090	244	240	13.7	13.5	17.4	17.1	21.1	20.7
28	44.80	2007.04	239.16	0.24	0.21	.2267	.2000	227	230	12.8	12.9	16.2	16.4	19.6	19.8
29	46.40	2152.96	222.95	0.22	0.19	.2090	.1819	209	209	11.8	11.8	14.9	14.9	18.0	18.0
30	48.00	2304.00	208.33	0.21	0.18	.2000	.1728	200	199	11.3	11.2	14.3	14.2	17.3	17.1
	DF-L No.1		(P&T)			<i>F_c</i> = 1000		<i>E</i> = 1.6							
	DF-L No.1 & Btr		Dim.Lum			<i>F_c</i> = 1500		<i>E</i> = 1.8							

Procedure for Analysis

1. calculate L_e/d_{min}
2. obtain F'_c
 - compute $F_{cE} = \frac{K_{cE} E}{\left(L_e/d\right)^2}$
 - $K_{cE}=0.3$ sawn
 - $K_{cE}=0.418$ glu-lam
3. compute $F_c^* \approx F_c C_D$
4. calculate F_{cE}/F_c^* and get C_p (table 14)
5. calculate $F'_c = F_c^* C_p$

Procedure for Analysis (cont'd)

6. compute $P_{allowable} = F'_c \cdot A$

- or find $f_{actual} = P/A$

7. is $P \leq P_{allowable}$? (or $f_{actual} \leq F'_c$?)

- yes: OK
- no: overstressed & no good

Procedure for Design

1. guess a size (pick a section)
2. calculate L_e/d_{\min}
3. obtain F'_c $F_{cE} = \frac{K_{cE} E}{\left(L_e/d\right)^2}$
 - compute
 - $K_{cE} = 0.3$ sawn
 - $K_{cE} = 0.418$ glu-lam
4. compute $F_c^* \approx F_c C_D$
5. calculate F_{cE}/F_c^* and get C_p (table 14)
6. calculate $F'_c = F_c^* C_p$

Procedure for Design (cont'd)

6. compute $P_{allowable} = F'_c \cdot A$

- or find $f_{actual} = P/A$

7. is $P \leq P_{allowable}$? (or $f_{actual} \leq F'_c$?)

- yes: OK
- no: pick a bigger section and **go back to step 2.**

LRFD design

- *limit states for failure*

$$P_u \leq \phi_c P_n$$

$$\phi_c = 0.85 \quad P_n = F_{cr} A_g$$

1. *yielding*

$$\lambda_c \leq 1.5$$

2. *buckling*

$$\lambda_c > 1.5$$

$$\lambda_c = \frac{KI}{r\pi} \sqrt{\frac{F_y}{E}} \quad L_e / r$$

λ_c – column slenderness parameter

A_g - gross area

Compact Sections

- *flanges continuously connected to the web or webs and width-thickness ratios < limiting values*
 - *no local buckling of flange or web*

– for $\lambda_c \leq 1.5$ $F_{cr} = \left(0.658^{\lambda_c^2}\right) F_y$

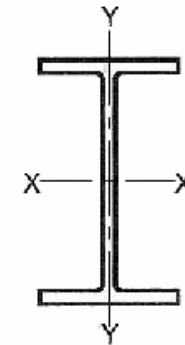
– for $\lambda_c > 1.5$ $F_{cr} = \left[\frac{0.877}{\lambda_c^2}\right] F_y$

Column Charts

$F_y = 50$ ksi

$\phi_c P_n = 0.85 F_{cr} A_g$

**Table 4-2 (cont.).
W-Shapes
Design Strength in Axial
Compression, $\phi_c P_n$, kips**



Shape	W10				W12				W14			
	106	96	87	79	72	65††	58	53	50	45	40	
0	1330	1200	1090	986	897	812	723	663	621	557	497	
6	1280	1150	1050	947	861	779	680	623	562	504	450	
7	1260	1140	1030	933	848	767	666	610	543	486	434	
8	1240	1120	1010	917	834	754	649	594	521	466	416	
9	1210	1100	994	900	818	739	631	577	497	445	396	
10	1190	1070	973	880	800	723	611	559	472	422	376	
11	1160	1050	950	860	781	706	590	539	445	398	354	
12	1130	1020	926	838	761	687	568	518	418	374	332	
13	1100	995	901	814	740	668	545	496	390	349	310	
14	1070	966	874	790	717	647	521	474	363	324	287	