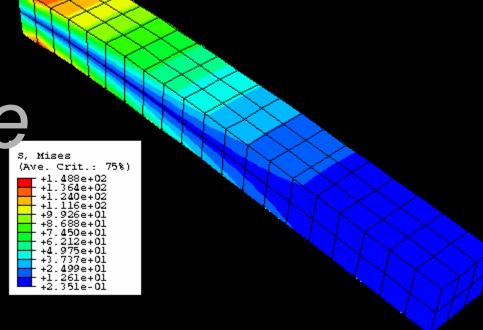
ARCHITECTURAL STRUCTURES I:

STATICS AND STRENGTH OF MATERIALS ENDS 231

DR. ANNE NICHOLS

SPRING 2007

twenty one

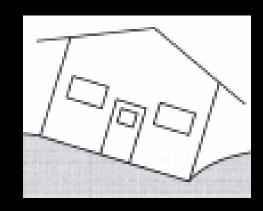


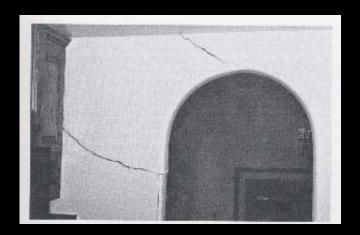
beams:

deflection & design

Design for Strength +...

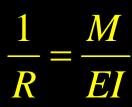
- strength design
 - forces & material
- serviceability
 - limit deflection and cracking
 - control noise & vibration
 - no excessive settlement of foundations
 - durability
 - appearance
 - component damage
 - ponding

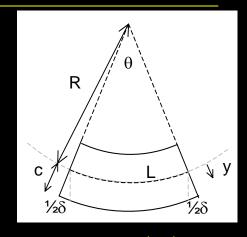




Beam Deformations

- curvature relates to
 - bending moment
 - modulus of elasticity
 - moment of inertia





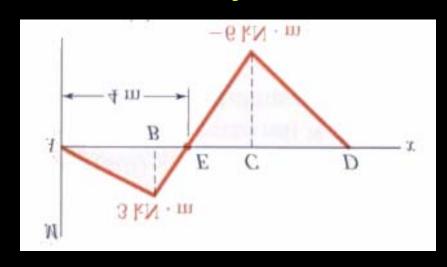
$$curvature = \frac{M(x)}{EI}$$

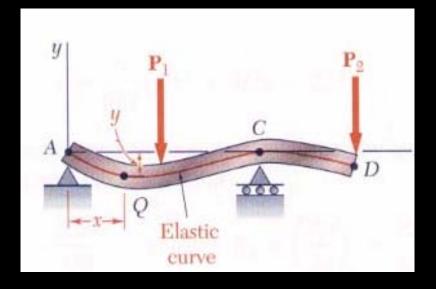
$$\theta = slope = \int \frac{M(x)}{EI} dx$$

$$\Delta = deflection = \int \int \frac{M(x)}{EI} dx$$

Deflected Shape & M(x)

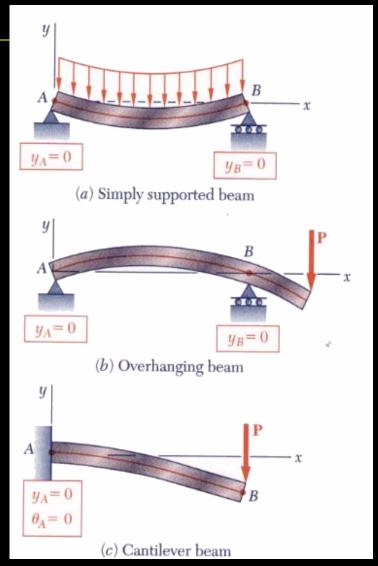
- -M(x) gives shape indication
- boundary conditions must be met





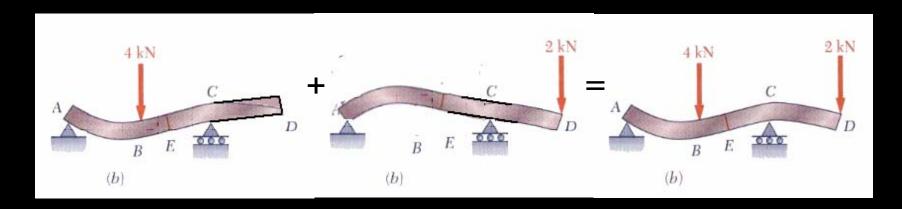
Boundary Conditions

- at pins, rollers, fixed supports: y = 0
- at fixed supports: $\theta = 0$
- at inflection points from symmetry: $\theta = 0$
- y_{max} at $\frac{dy}{dx} = 0$



Superpositioning

- if w can be superpositioned
 - $-\theta$ & y can
 - elastic range only!



Deflection Limits

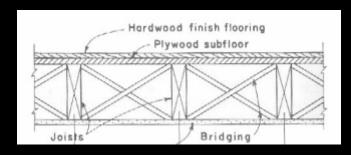
• based on service condition, severity

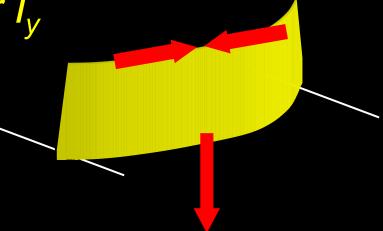
Use	LL only	DL+LL
Roof beams:		
Industrial	L/180	L/120
Commercial		
plaster ceiling	L/240	L/180
no plaster	L/360	L/240
Floor beams:		
Ordinary Usage	L/360	L/240
Roof or floor (damageable elements)		L/480

Lateral Buckling

- lateral buckling caused by compressive forces at top coupled with insufficient rigidity
- can occur at low stress levels

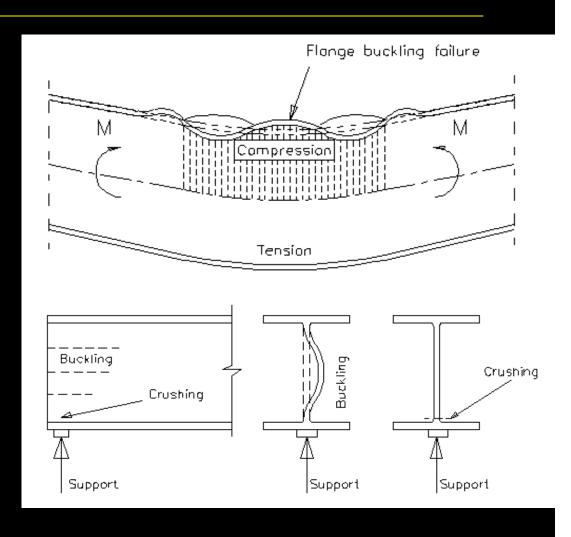
stiffen, brace or bigger I_y





Local Buckling

- steel I beams
- flange
 - buckle in direction of smaller radius of gyration
- web
 - force
 - "crippling"



Local Buckling

• flange

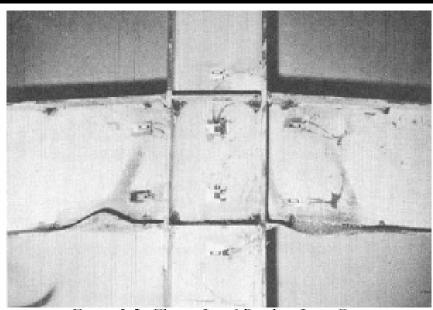


Figure 2-5. Flange Local Bending Limit State (Beedle, L.S., Christopher, R., 1964)

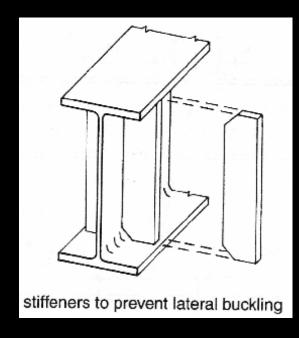
web

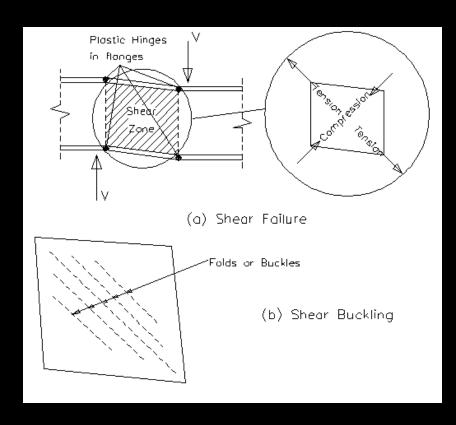


Figure 2-7. Web Local Buckling Limit State (SAC Project)

Shear in Web

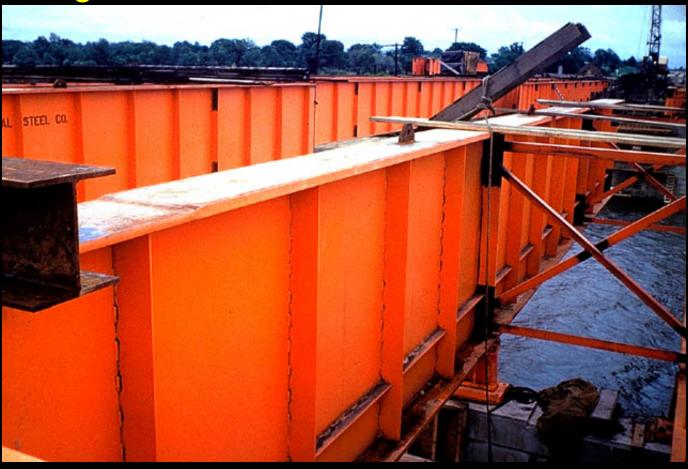
- panels in plate girders or webs with large shear
- buckling in compression direction
- add stiffeners



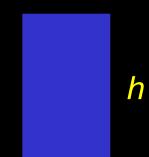


Shear in Web

• plate girders and stiffeners



- 1. Know F_{all} for the material or F_{U} for LRFD
- 2. Draw V & M, finding M_{max}



3. Calculate $S_{req'd}$ $(f_b \leq F_b)$

b

4. Determine section size

$$S=\frac{bh^2}{6}$$

- 4^* . Include self weight for M_{max}
 - and repeat 3 & 4 if necessary

5. Consider lateral stability

Unbraced roof trusses were blown down in 1999 at this project in Moscow, Idaho.

Photo: Ken Carper



6. Evaluate shear stresses - horizontal

•
$$(f_v \leq F_v)$$

W and rectangles

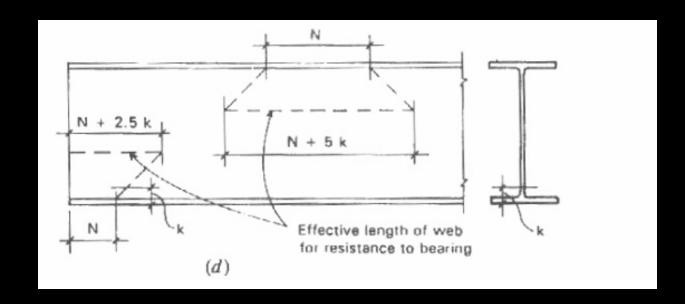
$$f_{v-\text{max}} = \frac{3V}{2A} \approx \frac{V}{A_{web}}$$

• thin walled sections

$$f_{v-\text{max}} = \frac{VQ}{Ib}$$

7. Provide adequate bearing area at supports

$$f_p = \frac{P}{A} \le F_p$$



8. Evaluate torsion

$$(f_v \leq F_v)$$

circular cross section

$$f_v = \frac{T\rho}{J}$$

rectangular

$$f_{v} = \frac{1}{c_{1}ab^{2}}$$

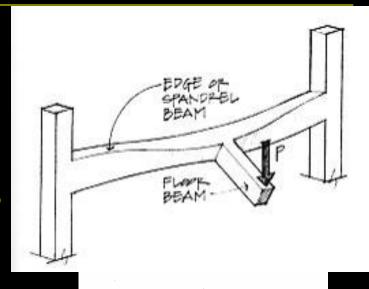
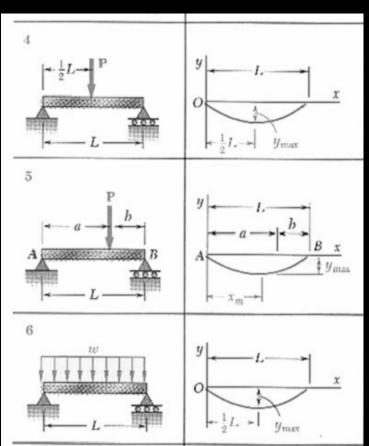
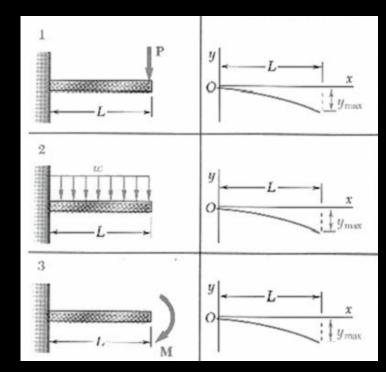


TABLE 3.1. Coefficients for Rectangular Bars in Torsion

a/b	c ₁	C ₂
1.0	° 0.208	0.1406
1.2	0.219	0.1661
1.5	0.231	0.1958
2.0	0.246	0.229
2.5	0.258	0.249
3.0	0.267	0.263
4.0	0.282	0.281
5.0	0.291	0.291
10.0	0.312	0.312
∞	0.333	0.333

9. Evaluate deflections

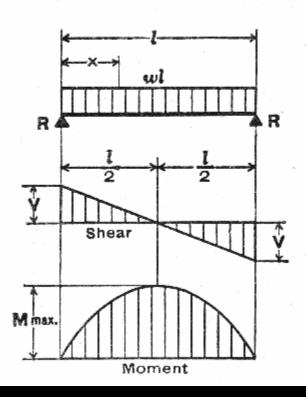




$$y_{\text{max}}(x) = \Delta_{actual} \le \Delta_{allowable}$$

9. – how to read charts

SIMPLE BEAM—UNIFORMLY DISTRIBUTED LOAD



Total Equiv. Uniform Load . . . =
$$wl$$

R = V = $\frac{wl}{2}$

Vx = $w\left(\frac{l}{2} - x\right)$

M max. (at center) . . . = $\frac{wl^2}{8}$

Mx = $\frac{wx}{2}(l - x)$
 Δmax . (at center) . . . = $\frac{5wl^4}{384 \text{ El}}$
 Δx = $\frac{wx}{24 \text{El}}(l^3 - 2lx^2 + x^3)$