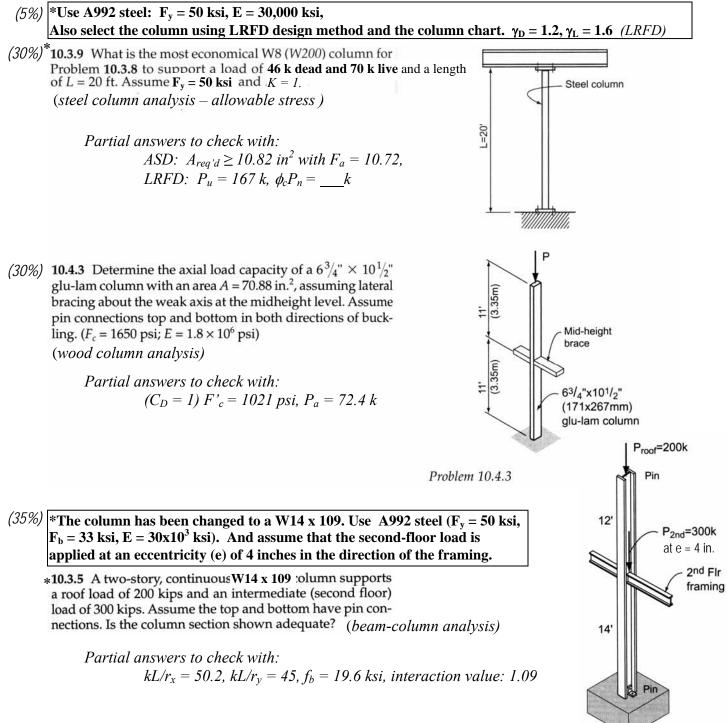
Pass-fail work

ENDS 231. Assignment #11

Date: 4/10/08, *due* 4/17/08

Problems: from Onouye, Chapter 10.

Note: Problems marked with a * have been altered with respect to the problem stated in the text.



Problem 10.3.5

| _ | $F_{y} = 36 \text{ ks}$ | | | | | | | | | | | | | | | | |
|--|-------------------------|--------------|---------------------|--------------|----------|--------------|--------|--------------|----------|--------------|------|--------------|----------|--------------------------------------|------------|--------------------------------------|-----------|
| x— | | x | COLUMNS W shapes | | | | | | | | | | | | | | |
| = | ļ | Ê. | De | sign | axia | stre | ngth | in kip | os (¢ | = 0.8 | 35) | | | | | | |
| esigr | nation | W8 | | | | | | | | | | | | W8 | | | |
| Wt./ft | | 67 | | 58 | | 48 | | 40 | | 35 | | 31 | | 28 | | 24 | |
| F | y | 36 | 50 | 36 | 50 | 36 | 50 | 36 | 50 | 36 | 50 | 36 | 50 | 36 | 50 | 36 | 50 |
| | 0 | 603 | 837 | 523 | 727 | 431 | 599 | 358 | 497 | 315 | 438 | 279 | 388 | 252 | 351 | 217 | 301 |
| Ś | 6 | 567 | 770 | 492 | 667 | 405 | 549 | 335 | 454 | 295 | 399 | 261 | 354 | 228 | 303 | 195 | 260 |
| | 7 | 555 | 746 | 481 | 647 | 396 | 532 | 327 | 439 | 288 | 386 | 255 | 342 | 219 | 288 | 188 | 247 |
| L. | 8 | 541 | 721 | 469 | 624 | 386 | 513 | 319 | 423 | 280 | 372 | 248 | 329 | 210 | 271 | 180 | 232 |
| atic | 9 | 526 | 693 | 455 | 599 | 374 | 492 | 309 | 405 | 272 | 356 | 240 | 315 | 200 | 253 | 171 | 217 |
| gyration | 10 | 509 | 662 | 441 | 572 | 362 | 470 | 298 | 386 | 262 | 339 | 232 | 300 | 189 | 235 | 162 | 200 |
| sof | 11 | 492 | 631 | 425 | 544 | 349 | 446 | 287 | 366 | 252 | 321 | 223 | 284 | 178 | 216 | 152 | 184 |
| radius | 12 | 473 | 598 | 409 | 515 | 335 | 422 | 275 | 345 | 242 | 303 | 214 | 268 | 167 | 197 | 142 | 16 |
| rac | 13 | 453 | 564 | 391 | 485 | 321 | 397 | 263 | 324 | 231 | 284 | 204 | 251 | 155 | 178 | 132 | 15 |
| ast | 14 | 433 | 529 | 374 | 455 | 306 | 372 | 251 | 303 | 220 | 265 | 194 | 234 | 143 | 160 | 122 | 13 |
| o les | 15 | 412 | 494 | 355 | 425 | 291 | 347 | 238 | 281 | 208 | 246 | 184 | 217 | 132 | 142 | 112 | 12 |
| ct | 16 | 391 | 460 | 337 | 394 | 276 | 321 | 225 | 260 | 197 | 228 | 174 | 200 | 121 | 125 | 102 | 10 |
| be | 17 | 370 | 425 | 318 | 365 | 260 | 297 | 211 | 239 | 185 | 209 | 163 | 184 | 110 | 111 | 93 | 9 |
| res | 18 | 349 | 392 | 300 | 335 | 245 | 272 | 198 | 219 | 174 | 191 | 153 | 168 | 99 | 99 | 84 | 8 |
| £ | 19 | 328 | 359 | 281 | 307 | 229 | 249 | 185 | 199 | 162 | 174 | 143 | 153 | 89 | 89 | 75 | 7! |
| (ft) with respect to least | 20 | 307 | 328 | 263 | 279 | 214 | 226 | 173 | 180 | 151 | 157 | 133 | 138 | 80 | 80 | 68 | 6 |
| К | 22 | 266 | 271 | 228 | 231 | 185 | 187 | 148 | 149 | 129 | 130 | 114 | 114 | 66 | 66 | 56 | 5 |
| 4 | 24 | 228 | 228 | 194 | 194 | 157 | 157 | 125 | 125 | 109 | 109 | 96 | 96 | 56 | 56 | 47 | 4 |
| g | 26 | 194 | 194 | 165 | 165 | 134 | 134 | 107 | 107 | 93 | 93 | 82 | 82 | 51 | 51 | 44 | 4 |
| lei | 28 | 167 | 167 | 143 | 143 | 115 | 115 | 92 | 92 | 80 | 80 | 70 | 70 | 47 | 47 | 40 | 4 |
| Effective length | 30 | 146 | 146 | 124 | 124 | 100 | 100 | 80 | 80 | 70 | 70 | 61 | 61 | 44 | 44 | | |
| Effe | 32 | 128 | 128 | 109 | 109 | 88 | 88 | 70 | 70 | 61 | 61 | 54 | 54 51 | | | | |
| | 33 | 120 | 120 | 103 | 103 | 83 | 83 | 66 62 | 66 62 | 58 | 58 | 51 | 51 | | 1. 241.24 | | |
| | 34 35 | 113 107 | 113 107 | 97 91 | 97 91 | 78 | 78 | 62 | 02 | | 1.67 | | - | | | | 1.1 |
| | 35 | 107 | 107 | 91 | 91 | Prop | erties | | | | | | 1 | 0.47 | 1.07 | | P |
| 1 | | 2.03 | 1.96 | 2 | 1.93 | 1.97 | 1.87 | 1.93 | 1.8 | 1.89 | 1.74 | 1.85 | 1.65 | 2.17 48 | 1.87 67 | 2.07 39 | 1.7 54 |
| u P _{wo} (kips) | | 147 | 205 | 120 | 167 | 86 | 119 | 69 | 96 | 56 | 78 | 48 | 67 | 10 | 14 | 9 | 12 |
| Pwi (kips/in.) | | 21 | 28 | 18 | 26 | 14 | 20 | 13 | 18 | 11 | 16 | 10 | 14 | 81 | 95 | 52 | 61 |
| Pwb (kips) | | 648 | 764 | 464 | 547 | 224 | 264 | 163 | 192 | 104 | 123 | 81 | 95 | 44 | 61 | 32 | 45 |
| Ph (kips) | | 177 | 246 | 133 | 185 | 95 | 132 | 64 | 88 | 50 | 69 | 38 | 53 | 6.8 | 5.7 | 6.7 | 5.7 |
| p (ft) | | 8.8 | 7.5 | 8.8 | 7.4 | 8.7 | 7.4 | 8.5 | 7.2 | 8.5 | 7.2 | 8.4 | 7.1 | 27.2 | 18.8 | 24.3 | 17. |
| L, (ft) | | 64.0 41.9 | | 55.9 36.8 | | 46.7 31.1 | | 39.1 26.5 | | 35.1 24.1 | | 32.0 22.4 | | 8.25 | | 7.08 | |
| A (in. ²) | | 19.7 | | 17.1 | | 14.1 | | 11.7 | | 10.3 | | 9.13 | | 98.0 21.7 1.62 2.13 2810 | | 82.8 18.3 1.61 2.12 2370 | |
| I _x (in. ⁴) | | 272 | | 228 | | 184 | | 146 | | 127 | | 110 | | | | | |
| I _y (in. ⁴) | | 88.6 | | 75.1 | | 60.9 | | 49.1 | | 42.6 | | 37.1 | | | | | |
| ry (in.) | | 2.12 | | 2.10 | | 2.08 | | 2.04 1.73 | | 2.03 | | 2.02 1.72 | | | | | |
| Ratio r_x / r_y $P_{ex} (KL)^2 / 10^4$ | | 1.75 | | 1.74 6520 | | 1.74 5260 | | 4170 | | 1.73 3630 | | 3150 | | 620 | | 2370 525 | |
| $P_{ex}(KL)^{2} / 10^{4}$ $P_{ey}(KL)^{2} / 10^{4}$ | | 7800 2530 | | 2160 | | 1750 | | 1390 | | 1210 | | | | ompact; see discussion precedi | | _ | |
| ey (AL | ., , 10 | 1000 | tes K1 / | | | | | 10 | | 12 | | 10 | | mpact, S | ee discus | sion prece | guing |