

### Examples: Beams (V, M, Stresses and Design)

#### Example 1

#### Example Problem 9.5: Section Modulus (Figures 9.26 to 9.28)

Two C10×15.3 steel channels are placed back to back to form a 10"-deep beam. Determine the permissible  $P$  if  $F_b = 30$  ksi. Assume A572 grade 50 steel.

**Solution:**

$$I_x = 67.4 \text{ in.}^4 \times 2 = 134.8 \text{ in.}^4$$

$$M_{\max} = \frac{1}{2}(5)(5) + (P/2)(5)$$

$$M_{\max} = 12.5 + 2.5P$$

$$= (12.5 \text{ k-ft.} + 2.5P) \times (12 \text{ in./ft.})$$

$$f = \frac{Mc}{I} = \frac{M}{S}; \quad \therefore M = F_b \times S_x$$

$$S_x = 2 \times 13.5 \text{ in.}^3 = 27 \text{ in.}^3$$

Equating both  $M_{\max}$  equations:

$$M = (30 \text{ k/in.}^2) \times (27 \text{ in.}^3) = 810 \text{ k-in.}$$

$$(12.5 \text{ k-ft.} + 2.5P)(12 \text{ in./ft.}) = 810 \text{ k-in.}$$

Dividing both sides of the equation by 12 in./ft.:

$$(12.5 \text{ k-ft.}) + (2.5 \text{ ft.})P + 67.5 \text{ k-ft.}$$

$$2.5P = 55 \text{ k}$$

$$\therefore P = 22 \text{ k}$$

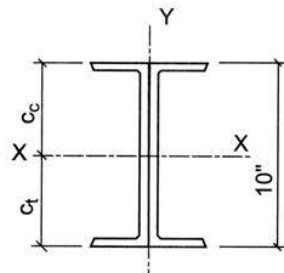


Figure 9.27 Beam cross-section.

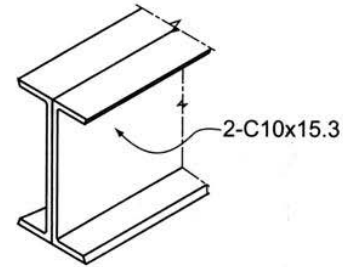


Figure 9.26 Two steel channels.

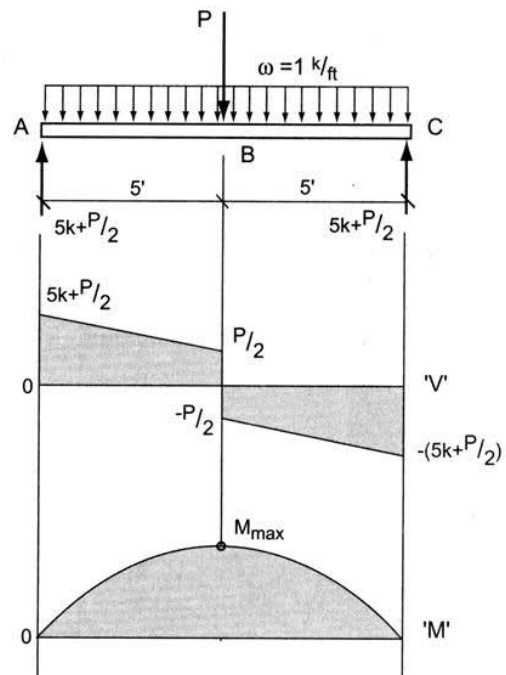


Figure 9.28 Load, V, and M diagrams.


Example 2 From eStructures v1.1, Shodek and Pollalis, 2000 Harvard College

Beam Analysis

STEP 1

**BEAM ANALYSIS**

Determine the bending and shear stresses in the timber beam shown. Also determine the deflections present. Is the beam adequately sized? Assume that the allowable bending stresses is  $F_{b,allowable} = 1500 \text{ lbs/in}^2$ , the allowable shear stress is  $F_{v,allowable} = 150 \text{ lbs/in}^2$ , and the allowable deflection is  $L/360$ . Also assume that the allowable stress in bearing is  $f_{bg} = 400 \text{ lbs/in}^2$  and  $E = 1.6 \times 10^6 \text{ lbs/in}^2$



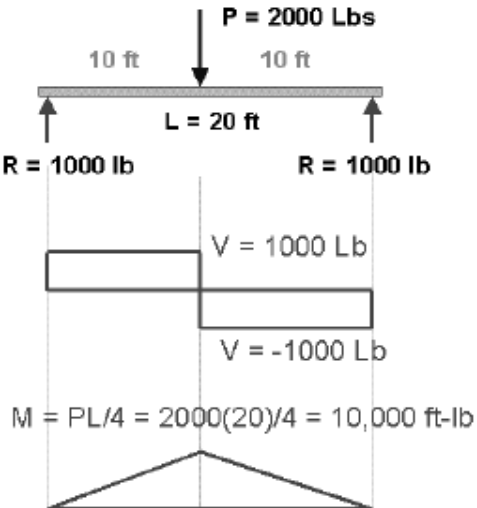
**CHECK BENDING, SHEAR, BEARING STRESSES AND DEFLECTIONS**

*Reference: eStructures v1.1, Shodek & Pollalis, 2000  
Simple Beams, Beam Analysis*

Beam Analysis

STEP 2

**DRAW SHEAR AND MOMENT DIAGRAMS**



**SHEAR AND MOMENT DIAGRAMS:**

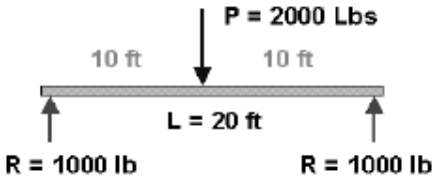
Maximum Shear Force:  
= 1000 lbs

Maximum Bending Moment:  
= 10,000 ft-lbs = 120,000 in-lbs

## Example 2 (continued)


Beam Analysis
STEP 3

DETERMINE BEAM PROPERTIES



$P = 2000 \text{ Lbs}$   
 $L = 20 \text{ ft}$   
 $R = 1000 \text{ lb}$

$b = 4 \text{ in}$



$c = d/2$   
 $d = 12 \text{ in}$

**MOMENT OF INERTIA:**

$$I = bd^3/12 = (4)(12)^3/12 = 576 \text{ in}^4$$

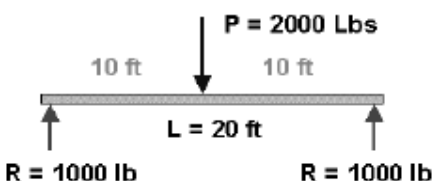
**SECTION MODULUS:**

$$S = I / c = 576 / (12/2) = 96 \text{ in}^3$$

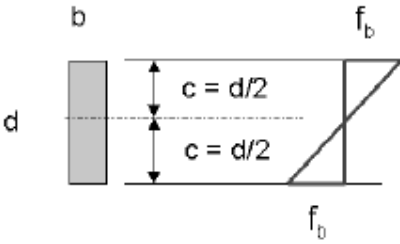
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Beam Analysis
STEP 4

BENDING STRESSES



$P = 2000 \text{ Lbs}$   
 $L = 20 \text{ ft}$   
 $R = 1000 \text{ lb}$



$c = d/2$   
 $c = d/2$   
 $f_b$

**BENDING STRESSES:**

$$f_b = M / S = (120,000 \text{ in-lb}) / 96 \text{ in}^3$$

$$= 1250 \text{ lb/in}^2$$

**CHECK:**  
1250 < 1500    OKAY IN BENDING

## Example 2 (continued)

**Beam Analysis** STEP 5

### SHEAR STRESSES

$P = 2000 \text{ Lbs}$   
 $L = 20 \text{ ft}$   
 $R = 1000 \text{ lb}$

$b$   
 $d$   
 $c = d/2$   
 $c = d/2$

**SHEAR STRESS =  $f_v = VQ/It$**   
For a **RECTANGULAR SECTION ONLY**,  
the maximum shear stress becomes:

$$f_v = (3/2) V/A = (3/2) V / bd$$

**SHEAR STRESSES:**

$$f_v = (3/2) V/A$$

$$= (3/2) (1000 \text{ lb}) / (4 \text{ in} \times 12 \text{ in})$$

$$= 31.25 \text{ lb/in}^2$$

**CHECK:**  
 $31.25 < 150$     OKAY IN SHEAR

**Beam Analysis** STEP 6

### BEARING STRESSES

$P = 2000 \text{ Lbs}$   
 $L = 20 \text{ ft}$   
 $R = 1000 \text{ lb}$

$b = 4 \text{ in}$   
 $t = 6 \text{ in}$

Assume that the beam rests on walls that are 6 inches wide. Thus, the bearing area at the reaction is  $4 \times 6 = 24 \text{ sq.in.}$

**BEARING STRESSES:**

$$f_{bg} = R/A$$

$$= 1000 \text{ lb} / 4 \text{ in} \times 6 \text{ in}$$

$$= 41.2 \text{ lb/in}^2$$

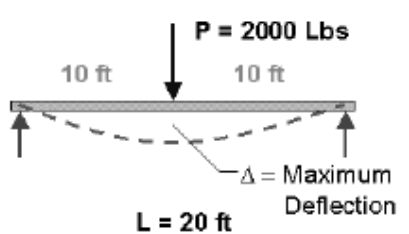
**CHECK:**  
 $41.2 < 400$     OKAY IN BEARING

## Example 2 (continued)

Beam Analysis
STEP 7

**DEFLECTIONS**

For a simply supported beam with a concentrated load, the maximum deflection is given by  $\Delta = PL^3/48EI$ :



$$\Delta = PL^3/48EI$$

$$= \frac{(2000 \text{ lb})(20 \text{ ft} \times 12 \text{ in/ft})^3}{48 (1.6 \times 10^6 \text{ lb/in}^2)(576 \text{ in}^4)}$$

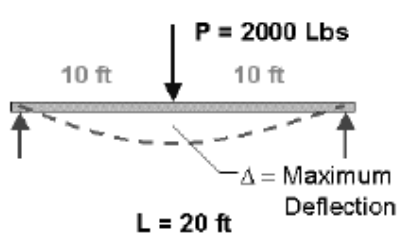
$$= 0.625 \text{ inches}$$

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Beam Analysis
STEP 8

**DEFLECTIONS**

For a simply supported beam with a concentrated load, the maximum deflection is given by  $\Delta = PL^3/48EI$ :



$$\Delta = PL^3/48EI$$

$$= \frac{(2000 \text{ lb})(20 \text{ ft} \times 12 \text{ in/ft})^3}{48 (1.6 \times 10^6 \text{ lb/in}^2)(576 \text{ in}^4)}$$

$$= 0.625 \text{ inches}$$

**COMPARE ACTUAL DEFLECTION TO ALLOWABLE DEFLECTION:**

$\Delta_{\text{actual}} = 0.625 \text{ in}$

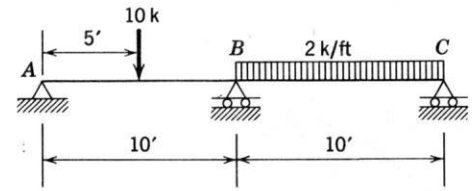
$\Delta_{\text{allowable}} = L / 360 = (20 \text{ ft} \times 12 \text{ in/ft}) / 360 = 0.67 \text{ in.}$

$\Delta_{\text{actual}} < \Delta_{\text{allowable}}$

Deflections are okay!

**Example 3**

Using an “approximate” method of analysis (specifically beam diagrams and formulas with superpositioning), find reactions, shears, and moments present in the structure. Verify the solution using a computer-based structural analysis program (Multiframe4D).



**SOLUTION:**

The load cases can be divided into the two shown which correspond to beam diagrams 30 and 29 (mirrored).

Because the maximum moments **do not** occur at the same place, find the reactions to add up and construct the V & M diagrams. The moment diagram should look like the two diagrams (with one flipped) “added” together:

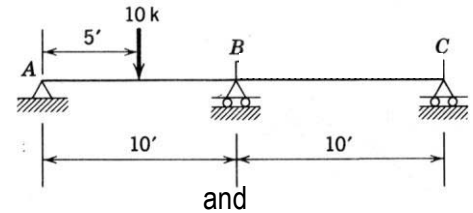


Diagram 30:

$$R_1 = \frac{13}{32} P = \frac{13}{32} (10k) = 4.06k \qquad R_2 = \frac{11}{16} P = \frac{11}{16} (10k) = 6.875k$$

$$R_3 = -\frac{3}{32} P = -\frac{3}{32} (10k) = -0.9375k$$

Diagram 29:

$$R_1 (was R_3) = -\frac{1}{16} wl = -\frac{1}{16} (2 \frac{k}{ft}) 10 ft = -1.25k \qquad R_2 = \frac{5}{8} wl = \frac{5}{8} (2 \frac{k}{ft}) 10 ft = 12.5k$$

$$R_3 (was R_1) = \frac{7}{16} wl = \frac{7}{16} (2 \frac{k}{ft}) 10 ft = 8.75k$$

Reaction sums:

$$R_1 = 4.06 + -1.25 = 2.81k \qquad R_2 = 6.875 + 12.5 = 19.375k \qquad R_3 = -0.9375 + 8.75 = 7.8125k$$

Shear calculations:

$$V_A = 0 \text{ and } 2.81k \qquad V_{at 5ft} = 2.81k \text{ and } 2.81 - 10 = -7.19k \qquad V_B = -7.19k \text{ and } -7.19 + 19.375 = 12.185k$$

$$V_C = 12.185 - 2k/ft(10ft) = -7.8125 \text{ and } -7.815 + 7.815 = 0k$$

Moment shapes:

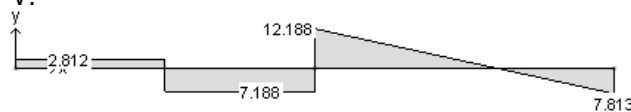
$$M_A = 0 \qquad M_{at 5ft} = 0 + 2.81k(5ft) = 14.05k\text{-ft} \qquad M_B = 14.05 - 7.19k(5ft) = -21.9k\text{-ft}$$

$$\text{location of cross over} = 12.185k / (2k/ft) = 6.0925ft: \qquad M_{at 6.1 ft from B} = -21.9 + 12.185k(6.0925ft) / 2 = 15.218 k\text{-ft}$$

$$M_C = 15.218 - 7.8125k(3.9075ft) / 2 = 0$$

MULTIFRAME4D:

V:



M:

