

Examples: Reinforced Concrete

Example 1

A simply supported beam 20 ft long carries a service dead load of 300 lb/ft and a live load of 500 lb/ft. Design an appropriate beam (for flexure only). Use grade 40 steel and concrete strength of 5000 psi.

SOLUTION:

Find the design moment, M_u , from the factored load combination of $1.2D + 1.6L$. It is good practice to guess a beam size to include self weight in the dead load, because "service" means dead load of everything except the beam itself.

Guess a size of 10 in x 12 in. Self weight for normal weight concrete is the density of 150 lb/ft³ multiplied by the cross section

$$\text{area: self weight} = 150 \frac{\text{lb}}{\text{ft}^3} (10 \text{ in})(12 \text{ in}) \cdot \left(\frac{1 \text{ ft}}{12 \text{ in}}\right)^2 = 125 \text{ lb/ft}$$

$$w_u = 1.2(300 \text{ lb/ft} + 125 \text{ lb/ft}) + 1.6(500 \text{ lb/ft}) = 1310 \text{ lb/ft}^2$$

The maximum moment for a simply supported beam

$$\text{is } \frac{wl^2}{8} :$$

$$M_u = \frac{w_u l^2}{8} = \frac{1310 \frac{\text{lb}}{\text{ft}} (20 \text{ ft})^2}{8} = 65,500 \text{ lb-ft}$$

$$M_n \text{ required} = M_u / \phi = \frac{65,500 \text{ lb-ft}}{0.9} = 72,778 \text{ lb-ft}$$

$$\text{To use the design chart aid, find } R_n = \frac{M_n}{bd^2},$$

estimating that d is about 1.75 inches less than h :

$$d = 12 \text{ in} - 1.75 \text{ in} = 10.25 \text{ in}$$

$$R_n = \frac{72,778 \text{ lb-ft}}{(10 \text{ in})(10.25 \text{ in})^2} \cdot \left(\frac{12 \text{ in}}{\text{ft}}\right) = 831 \text{ psi}$$

ρ corresponds to approximately 0.023, so the estimated area required, A_s , can be found:

$$A_s = \rho b d = (0.023)(10 \text{ in})(10.25 \text{ in}) = 2.36 \text{ in}^2$$

The number of bars for this area can be found from handy charts.

(Whether the number of bars actually fit for the width with cover and space between bars must also be considered.)

Try $A_s = 2.37 \text{ in}^2$ from 3#8 bars

$$d = 12 \text{ in} - 1.5 \text{ in (cover)} - \frac{1}{2} (8/8 \text{ in diameter bar}) = 10 \text{ in}$$

Find the moment capacity of the beam as designed, ϕM_n

$$a = A_s f_y / 0.85 f'_c b = 2.37 \text{ in}^2 (40 \text{ ksi}) / [0.85(5 \text{ ksi})10 \text{ in}] = 2.23 \text{ in}$$

$$\phi M_n = \phi A_s f_y (d - a/2) = 0.9 (2.37 \text{ in}^2) (40 \text{ ksi}) \left(10 \text{ in} - \frac{2.23 \text{ in}}{2}\right) \cdot \left(\frac{1}{12 \frac{\text{in}}{\text{ft}}}\right) = 63.2 \text{ k-ft} \approx 64 \text{ k-ft needed (not OK)}$$

So, we can increase d to 13 in, and $\phi M_n = 70.3 \text{ k-ft (OK)}$. Or increase A_s to 2 # 10's (2.54 in²), for $a = 2.39 \text{ in}$ and ϕM_n of 67.1 k-ft (OK).

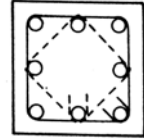
Table 3.7.1
Total Areas for Various Numbers of Reinforcing Bars

Bar Size	Nominal Diameter (in.)	Weight (lb/ft)	Number of Bars									
			1	2	3	4	5	6	7	8	9	10
#3	0.375	0.376	0.11	0.22	0.33	0.44	0.55	0.66	0.77	0.88	0.99	1.10
#4	0.500	0.668	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	2.00
#5	0.625	1.043	0.31	0.62	0.93	1.24	1.55	1.86	2.17	2.48	2.79	3.10
#6	0.750	1.502	0.44	0.88	1.32	1.76	2.20	2.64	3.08	3.52	3.96	4.40
#7	0.875	2.044	0.60	1.20	1.80	2.40	3.00	3.60	4.20	4.80	5.40	6.00
#8	1.000	2.670	0.79	1.58	2.37	3.16	3.95	4.74	5.53	6.32	7.11	7.90
#9	1.128	3.400	1.00	2.00	3.00	4.00	5.00	6.00	7.00	8.00	9.00	10.00
#10	1.270	4.303	1.27	2.54	3.81	5.08	6.35	7.62	8.89	10.16	11.43	12.70
#11	1.410	5.313	1.56	3.12	4.68	6.24	7.80	9.36	10.92	12.48	14.04	15.60
#14*	1.693	7.65	2.25	4.50	6.75	9.00	11.25	13.50	15.75	18.00	20.25	22.50
#18*	2.257	13.60	4.00	8.00	12.00	16.00	20.00	24.00	28.00	32.00	36.00	40.00

* #14 and #18 bars are used primarily as column reinforcement and are rarely used in beams.

Example 2

Determine the capacity of a 16" x 16" column with 8- #10 bars, tied. Grade 40 steel and 4000 psi concrete.



SOLUTION:

Find ϕP_n , with $\phi=0.65$ and $P_n = 0.80P_o$ for tied columns and

$$P_o = 0.85 f'_c (A_g - A_{st}) + f_y A_{st}$$

Steel area (found from reinforcing bar table for the bar size):

$$A_{st} = 8 \text{ bars} \times (1.27 \text{ in}^2) = 10.16 \text{ in}^2$$

Concrete area (gross):

$$A_g = 16 \text{ in} \times 16 \text{ in} = 256 \text{ in}^2$$

Grade 40 reinforcement has $f_y = 40,000$ psi and $f'_c = 4000$ psi

$$\phi P_n = (0.65)(0.80)[0.85(4000 \text{ psi})(256 \text{ in}^2 - 10.16 \text{ in}^2) + (40,000 \text{ psi})(10.16 \text{ in}^2)] = 646,026 \text{ lb} = 646 \text{ kips}$$

ASTM STANDARD REINFORCING BARS

Bar size, no.	Nominal diameter, in.	Nominal area, in. ²	Nominal weight, lb/ft
3	0.375	0.11	0.376
4	0.500	0.20	0.668
5	0.625	0.31	1.043
6	0.750	0.44	1.502
7	0.875	0.60	2.044
8	1.000	0.79	2.670
9	1.128	1.00	3.400
10	1.270	1.27	4.303
11	1.410	1.56	5.313
14	1.693	2.25	7.650
18	2.257	4.00	13.600