### ARCHITECTURAL STRUCTURES:

FORM, BEHAVIOR, AND DESIGN

ARCH 331

DR. ANNE NICHOLS

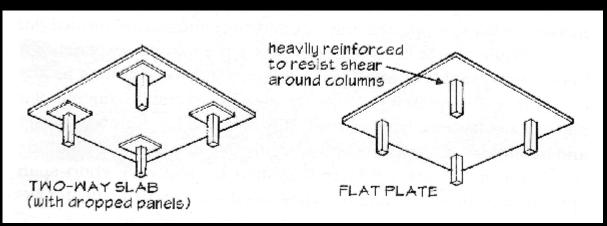
**F**ALL 2013

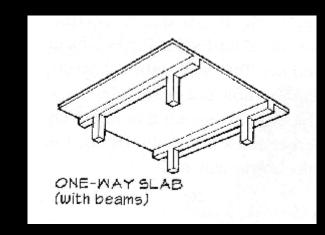
twenty three

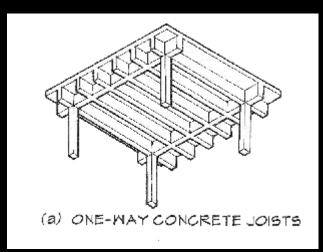


# Systems

- beams separate from slab
- beams integral with slab
  - close spaced
- continuous beams
- no beams







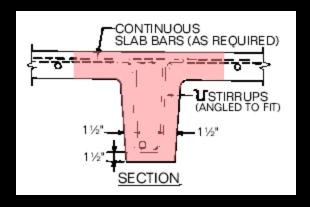
## T sections

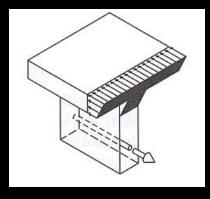
two areas of compression in moment

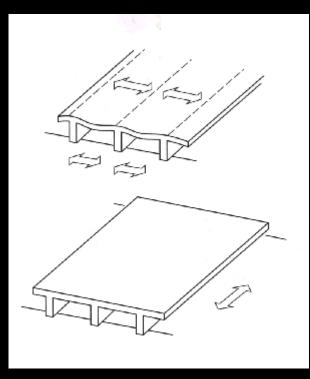
possible

one-way joists

effective flange width







### T sections

negative bending: min A<sub>s</sub>, larger of:

$$A_s = \frac{6\sqrt{f_c'}}{f_v}(b_w d) \qquad A_s = \frac{3\sqrt{f_c'}}{f_v}(b_f d)$$

- effective width (interior)
  - -L/4
  - $-b_{w} + 16t$
  - center-tocenter of beams

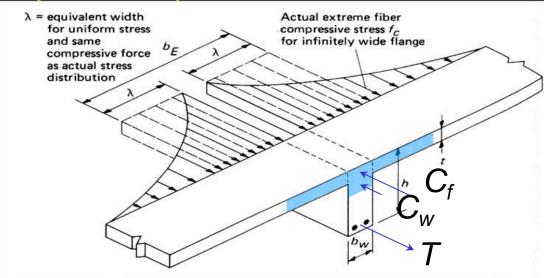
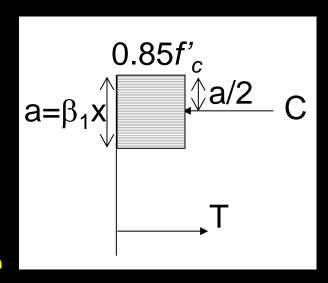


Figure 9.3.1 Actual and equivalent stress distribution over flange width.

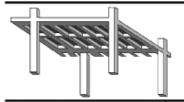
### T sections

- usual analysis steps
- 1. assume no compression in web
- 2. design like a rectangular beam
- 3. needs reinforcement in slab too
- 4. also analyze for negative moment, if any



# One-Way

- Joists
  - standard stems
  - 2.5" to 4.5" slab
  - − ~30" widths
  - reusable forms



#### **FLANGEforms**

FLANGEforms are available in standard 2- and 3-foot modules. These forms are among the most popular because of their flexibility to accommodate various layouts and joist widths where required. They are efficient for projects with heavy superimposed loads and provide a two hour fire rating by using a 4 1/2- inch hard-rock concrete topping. They are efficient for projects of smaller size and for moderate size projects with irregular layouts or unusual building shapes. They are also efficient for projects where the structure is not required to provide a two-hour fire rating by using 3-inch or 3 1/2-inch top slab.

The varying depths provide flexibility to meet a wide range of spans and loads. Further, they will accommodate in-the-floor raceway electrical and communication distribution systems. Ceco FLANGEforms are capable of producing sound structural concrete, but are incapable of producing tight tolerances and smooth finishes. This form is a seqmented steelform and the concrete will have irregular joists, a rough finish, and offsets at both the laps and flanges.

If a higher quality finish is required, you may wish to consider Ceco LONGforms (please see page 6.) The additional cost of higher quality forms are often offset by finishing costs. Contact your Ceco representative for assistance.

#### Concrete Quantities/30" Widths\*

Depth of	Width	Cablic feet of concr by slab to	ete per square foot Vickness*
Steelform	loiet	3"	41/2"
14"	5" 4" 7"	.456 .463 .508	.581. .608 .633
16"	6" 7" 8"	.512 .550 .557	.647 .675 .702
20"	6" 7" 8"	.605 .640 .674	.790 .765 .799
24"	6" 7" 8"	.694 .738 .776	.539 .581 .981

\* Apply only for areas over FLANGEforms and joists between them. Bridging joists, special headers, beam tees, etc., not included. 10" and 12" depths are also available. Contact your Ceco Concrete

#### Concrete Quantities/20" Widths\*

Depth of	Width of Joint	Cable fleet of concr for serious si	ete per square fixt ab frickness*
Soulform	loist	r	4 1/2"
14"	5" 6" 7"	.538 .572 .603	.663 .667 .728
16"	6" 7" 8"	/62.6 /662 /694	.751. .767 .839
20"	6" 7" 8"	.741 .765 .825	.867 .910 .950

Apply only for areas over FLANGEforms and joists between them. Bridging joists, special headers, beam tees, etc., not included. 10" and 12" depths are also available. Contact your Ceco Concrete Construction Engineer.





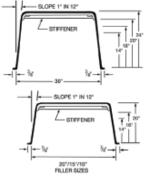
### Voids Created by Various Size

#### FLANGEforms

Shaded areas below indicate standard filler widths												
Depth of		et of void ore ry width of F	"Added Cu. Rt. of Concrete per Tapered End Condition									
Steelform	ser week	20" 84:35	11" No.05	11" No.26	set weath	32°Widh						
10"	2.023	1.129	.982	.63H	.521	.430						
12"	2.414	2.414 1.551		.748	.425	.500						
14"	2.801	2.801 1.629		.057	.730	N.A.						
16"	3.183	2.072	1.516	.964	.834	N.A.						
20"	3.933	2.544	1.850	1.155	1.043	N.A.						
24"	4.867	3.000	Not A	olatie	Hot Available							

from 30" to 25" or 20" to 16" in \*\* Total void width tapers





Concrete Slabs 6 Lecture 23

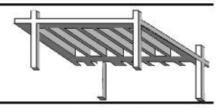
# One-Way

- Joists
  - wide pans
  - 5', 6' up
  - light loads & long spans
  - one-leg stirrups



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### WIDE FLANGEforms



WIDE FLANGEforms are available in standard 53 and 66-inch widths. When used with 7 and 6-inch joists they produce 5 and 6-foot modules respectively. ACI 318 requires the "joist" to be designed as a beam with minimum shear reinforcement. Any joist width can be used in combination with standard width pans to address span and load requirements. This system is very efficient for projects where the structural floor must provide a two-hour fire rating.

Using hard rock concrete, a 4 1/2-inch slab and minimum slab reinforcement will result in sufficient capacity for a variety of superimposed loads while reducing structure dead load. Shallower depth forms are appropriate for spans in the 25- to 35-foot range. Deeper depths are appropriate, under moderate loads, for spans in the 35- to 45-foot range using mild steel, while spans up to 60 feet can be achieved with post-tensioning.

By varying joist widths, different loading conditions can be accommodated using standard forming equipment without the need to add drop beams. Distribution ribs, which add unnecessary cost, are not required with wide module construction.

These forms are appropriate for structural concrete only, and should not be specified for critically exposed surfaces where appearance is important. They are a segmented steel form that will impart irregular lap and flange marks to the finished concrete, though many believe the finished product is acceptable for non-critically exposed work.

If a higher quality of finish is desired, for additional cost, you may wish to consider Ceco LONGforms (please see page 6). Your Ceco representative can assist in form type selection.





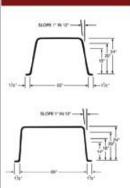
### Voids Created with 53" Design Module

Depth of Void	Cubic first of rold created per linear foot
14"	Not Arababie
16"	5.74L
20"	7.190
24"	8.590

#### Voids Created with 66" Design Module

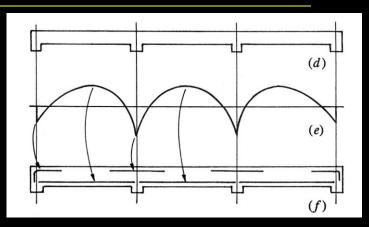
Depth of Void	Cubic Reet of void created per linear Root 6.303							
14"	4.303							
16"	7.185							
20"	8.995							
24"	10.667							

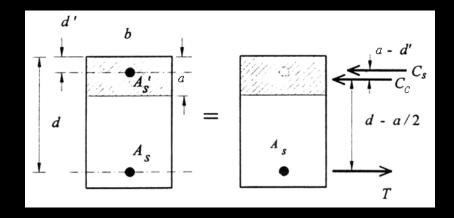
#### Dimensions



# Compression Reinforcement

- doubly reinforced
- negative bending
- two compression forces
- bigger M<sub>n</sub>
- control deflection
- increase ductility
- needs ties because of buckling





# Compression Reinforcement

## analysis

$$-A_s & A_s$$

$$-T = C_c + C_s$$

$$-T = A_s f_v$$

$$-C_s = A_s'(f'_s - 0.85f'_c)$$

$$-C_c = 0.85 f'_c$$
ba with  $a = \beta_1 x$ 

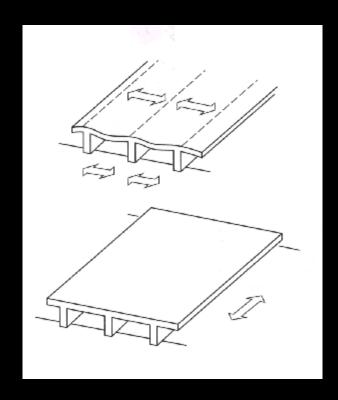
 $-f_s$  not known, so solve for x (n.a.)

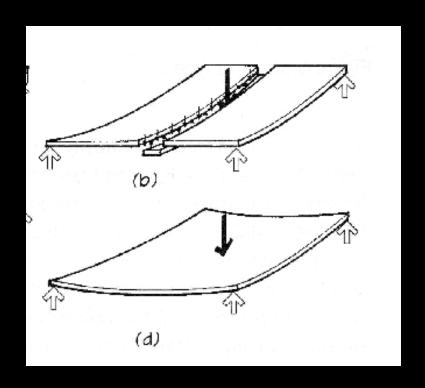
$$-f_{s}$$
'< $f_{v}$ ?

$$-M_n = T(d-a/2) + C_s(d-d')$$

### Slabs

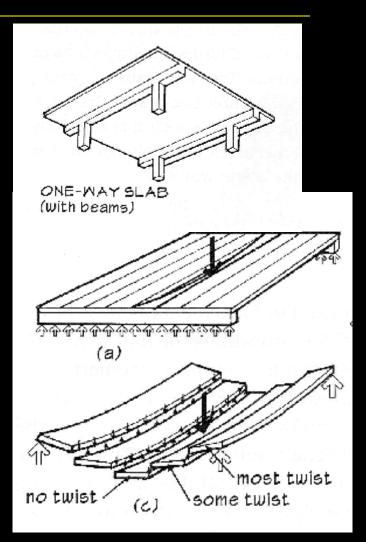
- one way behavior like beams
- two way behavior more complex





# Slab Design

- one unit wide "strip"
- with uniform loads
  - like "wide" beams
  - moment / unit width
  - uniform curvature
- with point loads
  - resisted by stiffness of adjacent strips
  - more curvature in middle



# Slab Design

- min thickness by code
- reinforcement
  - bars, welded wire mesh
  - cover
  - minimum by steel grade

$$\rho = \frac{A_s}{ht} = 0.002$$

• 60:

$$\rho = \frac{A_s}{bt} = 0.0018$$

# TABLE 9.5(a)—MINIMUM THICKNESS OF NONPRESTRESSED BEAMS OR ONE-WAY SLABS UNLESS DEFLECTIONS ARE COMPUTED

	PETON BROWN	Minimum tl							
1000	Simply sup- ported	Cantilever							
Member	Members not supporting or attached to partitions or other construction likely to be damaged by large deflections.								
Solid one- way slabs	ℓ/20	ℓ/24	ℓ/28	ℓ/10					
Beams or ribbed one- way slabs	ℓ/16	ℓ/18.5	ℓ /21	l /8					

#### Notes:

Values given shall be used directly for members with normalweight concrete and Grade 60 reinforcement. For other conditions, the values shall be modified as follows:

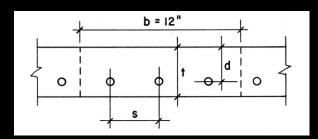
a) For lightweight concrete having equilibrium density,  $w_c$ , in the range of 90 to 115 lb/ft<sup>3</sup>, the values shall be multiplied by  $(1.65-0.005w_c)$  but not less than 1.09.

b) For  $f_y$  other than 60,000 psi, the values shall be multiplied by  $(0.4 + f_y f_100,000)$ .



# One-Way Slabs

- A<sub>s</sub> tables
- max spacing
  - $\le 3(t)$  and 18"



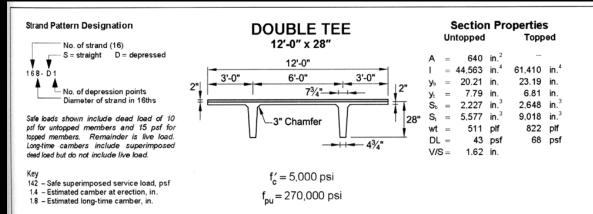
- $\le 5(t)$  and 18" temp & shrinkage steel
- no room for stirrups

Table 3-7 Areas of Bars pe	er Foot Width of Slab—As (in.2/ft)
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Bar	ar Bar spacing (in.)												
size	6	7	8	9	10	11	12	13	14	15	16	17	18
#3	0.22	0.19	0.17	0.15	0.13	0.12	0.11	0.10	0.09	0.09	0.08	0.08	0.07
#4	0.40	0.34	0.30	0.27	0.24	0.22	0.20	0.18	0.17	0.16	0.15	0.14	0.13
#5	0.62	0.53	0.46	0.41	0.37	0.34	0.31	0.29	0.27	0.25	0.23	0.22	0.21
#6	0.88	0.75	0.66	0.59	0.53	0.48	0.44	0.41	0.38	0.35	0.33	0.31	0.29
#7	1.20	1.03	0.90	0.80	0.72	0.65	0.60	0.55	0.51	0.48	0.45	0.42	0.40
#8	1.58	1.35	1.18	1.05	0.95	0.86	0.79	0.73	0.68	0.63	0.59	0.56	0.53
#9	2.00	1.71	1.50	1.33	1.20	1.09	1.00	0.92	0.86	0.80	0.75	0.71	0.67
#10	2.54	2.18	1.91	1.69	1.52	1.39	1.27	1.17	1.09	1.02	0.95	0.90	0.85
#11	3.12	2.67	2.34	2.08	1.87	1.70	1.56	1.44	1.34	1.25	1.17	1.10	1.04

### Precast

- prestressed
  - PCI DesignHandbook
  - double T's
  - hollow core
  - -L's
- topping
- load tables



. . . .

Normal Weight Concrete

12DT28 + 2

#### Table of safe superimposed service load (psf) and cambers (in.)

#### 2 in. Normal Weight Topping

Strand	y <sub>s</sub> (end) in.								8	pan, f	t								
Pattern	Pattern	y <sub>s</sub> (center) in.	40	42	44	46	48	50	52	54	56	58	60	62	64	66	68	70	72
	6.00	127	110	95	82	70	60	51	42	35	29								
108-S		8.0	0.9	0.9	0.9	0.9	0.9	0.9	8.0	8.0	0.7								
	6.00	8.0	0.8	8.0	0.8	0.7	0.6	0.5	0.3	0.1	-0.1								
-	7.00	154	134	117	102	88	77	66	57	49	41	32							
128-S	7.00 7.00	1.0	1.0	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1.0	0.9							
	7.00	1.0	1.0	1.0	1.0	1.0	0.9	0.8	0.7	0.5	0.3	0.0							
148-S	8.00 8.00	177	155	136	119	105	92	80	70	60	50	41	32						
		1.1	1.1	1.2	1.2	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.1						
		1.1	1.2	1.2	1.2	1.1	1.1	1.0	0.9	8.0	0.6	0.3	0.1						
200	9.00	197	173	152	134	118	104	90	78	66	56	47	39	31					
168-S		1.1	1.2	1.3	1.3	1.4	1.4	1.4	1.4	1.4	1.4	1.3	1.3	1.2					
	9.00	1.2	1.3	1.3	1.3	1.3	1.2	1.2	1.1	0.9	0.8	0.5	0.3	0.0					
	13.00			199	177	157	140	125	111	97	84	72	62	52	43	36	30		
168-D1				1.5	1.6	1.7	1.8	1.9	1.9	2.0	2.0	2.0	2.0	1.9	1.8	1.8	1.6		
100-01	3.75			1.7	1.7	1.7	1.8	1.7	1.7	1.6	1.5	1.3	1.1	0.8	0.5	0.2	-0.2		
in the second	14.39						(Coleba)	143	126	111	97	85	73	63	54	45	37	31	
188-D1								2.0	2.1	2.1	2.2	2.2	2.3	2.3	2.2	2.1	2.0	1.9	
8	4.00							1.9	1.9	1.9	1.8	1.7	1.5	1.3	1.0	0.7	0.3	-0.2	