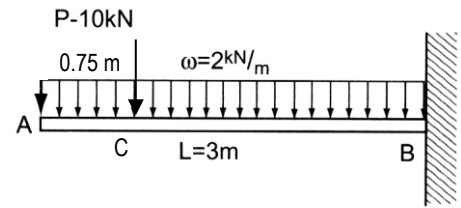


Example 1 (changed from pg 284) (superpositioning)

**Example Problem 8.5 (Semi-Graphical Method)**

A cantilever beam supports a uniform load of  $\omega = 2 \text{ kN/m}$  over its entire span, plus a concentrated load of 10 kN at the free end. Investigate using *Beam Diagrams and Formulas*.

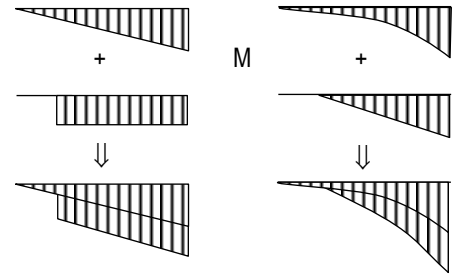


SOLUTION:

By examining the support conditions, we are looking for a cantilevered beam from Cases 18 through 23.

There is a case for uniformly distributed load across the span (19) and for a load at any point (21).

For both these cases, it shows that the maximum shear AND maximum moment are located at the fixed end. If we add the values, the shear and diagrams should look like this:



We can find the maximum shear (at B) from  $V = P + \omega l = 10 \text{ kN} + 2 \text{ kN/m} \cdot 3 \text{ m} = 16 \text{ kN}$

The maximum moment (at B) will be  $M = Pb + \omega l^2/2 = 10 \text{ kN} \cdot 2.25 \text{ m} + 2 \text{ kN/m} (3 \text{ m})^2/2 = 31.5 \text{ kN}\cdot\text{m}$

The key values for the diagrams can be found with the general equations ( $V_x$  and  $M_x$ ):

$$V_{C \leftarrow} = -\omega x = -2 \text{ kN/m} \cdot 0.25 \text{ m} = -0.5 \text{ kN}; \quad V_{C \rightarrow} = -P - \omega x = -10 \text{ kN} - 2 \text{ kN/m} \cdot 0.25 \text{ m} = -10.5 \text{ kN}$$

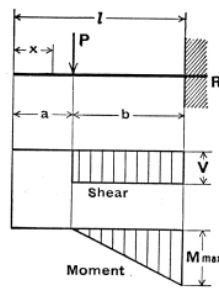
$$M_C = -\omega x^2/2 = 2 \text{ kN/m} (0.25 \text{ m})^2/2 = 0.0625 \text{ kN}\cdot\text{m}$$

We can find the maximum deflection by looking at the cases. Both say  $\Delta_{max}$  (at free end), so the values can be added directly. *Superpositioning of values must be at the same x location.* Assume  $E = 70 \times 10^3 \text{ MPa}$  and  $I = 45 \times 10^6 \text{ mm}^4$

$$\Delta_{total} = \frac{Pb^2}{6EI} (3l - b) + \frac{\omega l^4}{8EI} = \frac{10 \text{ kN} (2.25 \text{ m})^2 (10^3 \text{ mm/m})^3 (10^3 \text{ N/kN})}{6(70 \times 10^3 \text{ MPa})(45 \times 10^6 \text{ mm}^4)} (3 \cdot 3 \text{ m} - 2.25 \text{ m}) + \frac{2 \text{ kN/m} (3 \text{ m})^4 (10^3 \text{ mm/m})^3 (10^3 \text{ N/kN})}{8(70 \times 10^3 \text{ MPa})(45 \times 10^6 \text{ mm}^4)}$$

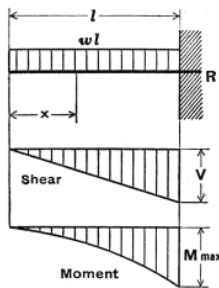
$$= 18.08 \text{ mm} + 6.43 \text{ mm} = 24.5 \text{ mm}$$

**21. CANTILEVER BEAM—CONCENTRATED LOAD AT ANY POINT**



Total Equiv. Uniform Load . . . . . =  $\frac{8Pb}{l}$   
 $R = V$  . . . . . =  $P$   
 $M$  max. (at fixed end) . . . . . =  $Pb$   
 $M_x$  (when  $x > a$ ) . . . . . =  $P(x - a)$   
 $\Delta_{max}$ . (at free end) . . . . . =  $\frac{Pb^2}{6EI} (3l - b)$   
 $\Delta_a$  (at point of load) . . . . . =  $\frac{Pb^3}{3EI}$   
 $\Delta_x$  (when  $x < a$ ) . . . . . =  $\frac{Pb^2}{6EI} (3l - 3x - b)$   
 $\Delta_x$  (when  $x > a$ ) . . . . . =  $\frac{P(l - x)^2}{6EI} (3b - l + x)$

**19. CANTILEVER BEAM—UNIFORMLY DISTRIBUTED LOAD**

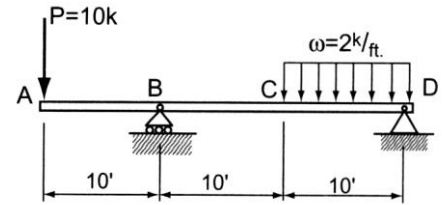


Total Equiv. Uniform Load . . . . . =  $4\omega l$   
 $R = V$  . . . . . =  $\omega l$   
 $V_x$  . . . . . =  $\omega x$   
 $M$  max. (at fixed end) . . . . . =  $\frac{\omega l^2}{2}$   
 $M_x$  . . . . . =  $\frac{\omega x^2}{2}$   
 $\Delta_{max}$ . (at free end) . . . . . =  $\frac{\omega l^4}{8EI}$   
 $\Delta_x$  . . . . . =  $\frac{\omega}{24EI} (x^4 - 4l^3x + 3l^4)$

**Example 2 (pg 275) (superpositioning)**

**Example Problem 8.2(Equilibrium Method)**

Draw  $V$  and  $M$  diagrams for an overhang beam (Figure 8.12) loaded as shown. Determine the critical  $V_{max}$  and  $M_{max}$  locations and magnitudes using *Beam Diagrams and Formulas*.

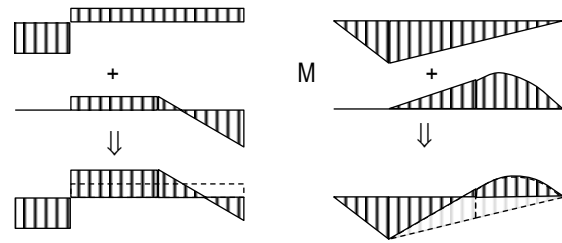


**SOLUTION:**

By examining the support conditions, we are looking for beam with an overhang on one end from Cases 24 through 28. (Even though the overhang is on the right, and not on the left like our beam, we can still use the information by recognizing that we can mirror the figure about the left end.)

There is a case for a load at the end (26) but none for a load in between the supports. This is because it behaves exactly like a simply supported beam in this instance (no shear or bending on the overhang). The case for this is #5 (reversed again).

If we “flip” the diagrams (both vertically and horizontally) and add the values, the resulting shear and bending moment should look like this:



We still have to find the peak values of shear and the location of the zero shear to find the critical moment values.

(Notice  $R_1$  is shown down.)

$$R_{1(D)} = -\frac{Pa}{l} + \frac{wa}{2l}(2l-a) = -\frac{10^k \cdot 10^{ft}}{20^{ft}} + \frac{2^{k/ft} \cdot 10^{ft}}{2 \cdot 20^{ft}}(2 \cdot 20^{ft} - 10^{ft}) = 10^k$$

$$R_{2(B)} = 10^{ft} + 2^{k/ft} \cdot 10^{ft} - 10^k = 20^k \quad (\text{from the total downward load} - R_{1(D)})$$

$$V_A = -10^k \quad V_B = -10^k + 20^k = 10^k$$

$$V_D = 10^k - 2^{k/ft}(10^{ft}) = -10^k$$

$$x \text{ (from B)} = 10^k / 2^{k/ft} = 5 \text{ ft}$$

$$M_B = -10^k(10^{ft}) = -100^k\text{-ft}$$

$$(M_C = -100^k\text{-ft} + 10^k(10^{ft}) = 0)$$

$$M_x = 0 + 10^k(5^{ft})/2 = 25^k\text{-ft}$$

$V_{MAX} = 10^k \quad M_{MAX} = -100^k\text{-ft}$

We can calculate the deflection between the supports. (And at the end for case 5 if we derive the slope!) Assume  $E = 29 \times 10^3 \text{ ksi}$  and  $I = 103 \text{ in}^4$

**26. BEAM OVERHANGING ONE SUPPORT—CONCENTRATED LOAD AT END OF OVERHANG**

$R_1 = V_1$	$= \frac{Pa}{l}$
$R_2 = V_1 + V_2$	$= \frac{P}{l}(l+a)$
$V_2$	$= P$
$M \text{ max. (at } R_2)$	$= Pa$
$M_x \text{ (between supports)}$	$= \frac{Pax}{l}$
$M_{x_1} \text{ (for overhang)}$	$= P(a-x_1)$
$\Delta_{max.} \text{ (between supports at } x = \frac{l}{\sqrt{3}})$	$= \frac{Pa^2}{9\sqrt{3}EI} = .06415 \frac{Pa^2}{EI}$
$\Delta_{max.} \text{ (for overhang at } x_1 = a)$	$= \frac{Pa^2}{3EI}(l+a)$
$\Delta_x \text{ (between supports)}$	$= \frac{Pax}{6EI l}(l^2-x^2)$
$\Delta_{x_1} \text{ (for overhang)}$	$= \frac{Px_1}{6EI}(2al+3ax_1-x_1^2)$

We'll investigate the maximum between the supports from case 26 (because it isn't obvious where the maximum will be.)

$$x = \frac{l}{\sqrt{3}} = \frac{20^{ft}}{\sqrt{3}} = 11.55^{ft} \text{ (to left of D) and } \Delta_{total} = \Delta_{max. - \text{case 26}} + \Delta_{x - \text{case 5}} \text{ with } x \text{ (11.55}^{ft}) \text{ greater than } a \text{ (10}^{ft})$$

$$\Delta_{total} = .06415 \frac{Pal^2}{EI} + \frac{wa^2(l-x)}{24EI l}(4xl - 2x^2 - a^2) \quad \text{Note: Because there is only negative moment, the deflection is actually up!}$$

$$= -.06415 \frac{10^k(10^{ft})(20^{ft})^2(12^{in/ft})^3}{(29 \cdot 10^3 \text{ ksi})(103 \text{ in}^4)} + \frac{2^{k/ft}(10^{ft})^2(20^{ft} - 10^{ft})}{24(29 \cdot 10^3 \text{ ksi})(103 \text{ in}^4)(20^{ft})} \times \dots$$

$$(4 \cdot 11.55^{ft} \cdot 20^{ft} - 2(11.55^{ft})^2 - (10^{ft})^2)(12^{in/ft})^3$$

$$= -1.484 \text{ in} + 1.343 \text{ in} = -0.141 \text{ in (up)}$$

**5. SIMPLE BEAM—UNIFORM LOAD PARTIALLY DISTRIBUTED AT ONE END**

$R_1 = V_1 \text{ max.}$	$= \frac{wa}{2l}(2l-a)$
$R_2 = V_2$	$= \frac{wa^2}{2l}$
$V_x \text{ (when } x < a)$	$= R_1 - wx$
$M \text{ max. (at } x = \frac{R_1}{w})$	$= \frac{R_1^2}{2w}$
$M_x \text{ (when } x < a)$	$= R_1x - \frac{wx^2}{2}$
$M_x \text{ (when } x > a)$	$= R_2(l-x)$
$\Delta_x \text{ (when } x < a)$	$= \frac{wx}{24EI l}(a^2(2l-a)^2 - 2ax^2(2l-a) + lx^3)$
$\Delta_x \text{ (when } x > a)$	$= \frac{wa^2(l-x)}{24EI l}(4xl - 2x^2 - a^2)$