

Beam Design and Deflections

Notation:

<p>a = name for width dimension</p> <p>A = name for area</p> <p>$A_{req'd-adj}$ = area required at allowable stress when shear is adjusted to include self weight</p> <p>A_{web} = area of the web of a wide flange section</p> <p>b = width of a rectangle = total width of material at a horizontal section = name for height dimension</p> <p>c = largest distance from the neutral axis to the top or bottom edge of a beam</p> <p>c_1 = coefficient for shear stress for a rectangular bar in torsion</p> <p>d = calculus symbol for differentiation</p> <p>DL = shorthand for dead load</p> <p>E = modulus of elasticity</p> <p>f_b = bending stress</p> <p>f_p = bearing stress (see P)</p> <p>f_v = shear stress</p> <p>f_{v-max} = maximum shear stress</p> <p>F_b = allowable bending stress</p> <p>F_v = allowable shear stress</p> <p>F_p = allowable bearing stress</p> <p>F_y = yield strength</p> <p>F_{yweb} = yield strength of the web material</p> <p>h = height of a rectangle</p> <p>I = moment of inertia with respect to neutral axis bending</p> <p>I_{trial} = moment of inertia of trial section</p> <p>$I_{req'd}$ = moment of inertia required at limiting deflection</p> <p>J = polar moment of inertia</p> <p>L = name for span length</p> <p>LL = shorthand for live load</p> <p>$LRFD$ = load and resistance factor design</p> <p>M = internal bending moment</p> <p>M_{max} = maximum internal bending moment</p>	<p>$M_{max-adj}$ = maximum bending moment adjusted to include self weight</p> <p>M_n = nominal flexure strength with the full section at the yield stress for LRFD</p> <p>M_u = maximum moment from factored loads for LRFD</p> <p>P = name for axial force vector</p> <p>Q = first moment area about a neutral axis</p> <p>R = radius of curvature of a deformed beam</p> <p>S = section modulus</p> <p>$S_{req'd}$ = section modulus required at allowable stress</p> <p>T = torque (axial moment)</p> <p>V = internal shear force</p> <p>V_{max} = maximum internal shear force</p> <p>$V_{max-adj}$ = maximum internal shear force adjusted to include self weight</p> <p>V_u = maximum shear from factored loads for LRFD</p> <p>w = name for distributed load</p> <p>$w_{self\ wt}$ = name for distributed load from self weight of member</p> <p>x = horizontal distance</p> <p>y = vertical distance</p> <p>Δ_{actual} = actual beam deflection</p> <p>$\Delta_{allowable}$ = allowable beam deflection</p> <p>Δ_{limit} = allowable beam deflection limit</p> <p>Δ_{max} = maximum beam deflection</p> <p>ϕ_b = resistance factor for flexure in LRFD design</p> <p>ϕ_v = resistance factor for shear for LRFD</p> <p>γ = density or unit weight</p> <p>θ = slope of the beam deflection curve</p> <p>ρ = radial distance</p> <p>\int = symbol for integration</p> <p>Σ = summation symbol</p>
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Criteria for Design

Allowable bending stress or bending stress from LRFD should not be exceeded:

$$F_b \geq f_b = \frac{Mc}{I}$$

Knowing M and F_b , the minimum section modulus fitting the limit is:

$$S_{req'd} \geq \frac{M}{F_b}$$

Besides strength, we also need to be concerned about *serviceability*. This involves things like limiting deflections & cracking, controlling noise and vibrations, preventing excessive settlements of foundations and durability. When we know about a beam section and its material, we can determine beam deformations.

Determining Maximum Bending Moment

Drawing V and M diagrams will show us the maximum values for design. Remember:

$$\begin{aligned} V &= \Sigma(-w)dx & \frac{dV}{dx} &= -w & \frac{dM}{dx} &= V \\ M &= \Sigma(V)dx \end{aligned}$$

Determining Maximum Bending Stress

For a prismatic member (constant cross section), the maximum normal stress will occur at the maximum moment.

For a *non-prismatic* member, the stress varies with the cross section AND the moment.

Deflections

If the bending moment changes, $M(x)$ across a beam of constant material and cross section then the curvature will change:

$$\frac{1}{R} = \frac{M(x)}{EI}$$

The slope of the n.a. of a beam, θ , will be tangent to the radius of curvature, R :

$$\theta = slope = \frac{1}{EI} \int M(x)dx$$

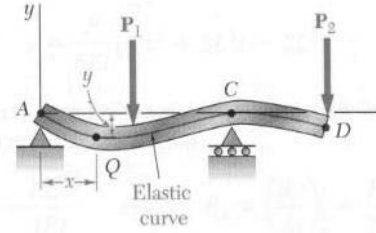
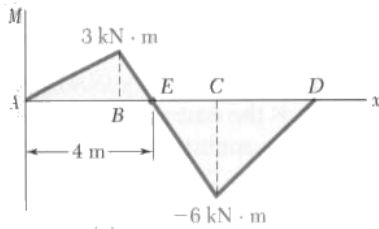
The equation for deflection, y , along a beam is:

$$y = \frac{1}{EI} \int \theta dx = \frac{1}{EI} \iint M(x)dx$$

Elastic curve equations can be found in handbooks, textbooks, design manuals, etc... Computer programs can be used as well. (BigBoy Beam freeware: <http://forum.simtel.net/pub/pd/33994.html>)

Elastic curve equations can be **superpositioned** ONLY if the stresses are in the elastic range.

The deflected shape is roughly the same shape as the bending moment diagram flipped but is constrained by supports and geometry.



Boundary Conditions

The boundary conditions are geometrical values that we know – slope or deflection – which may be restrained by supports or symmetry.

At Pins, Rollers, Fixed Supports: $y = 0$

At Fixed Supports: $\theta = 0$

At Inflection Points From Symmetry: $\theta = 0$

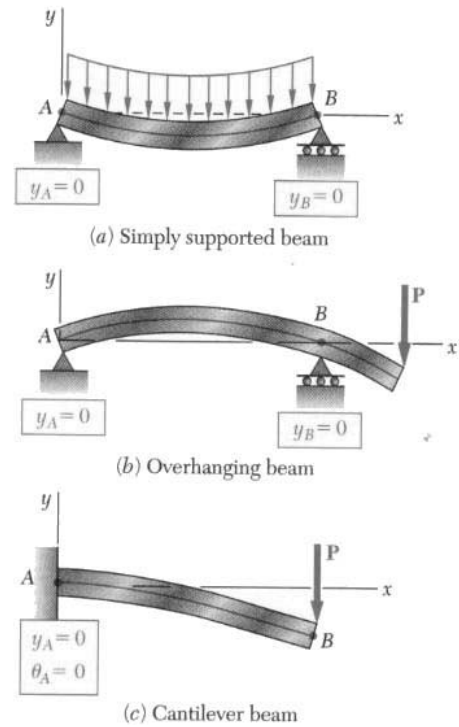
The Slope Is Zero At The Maximum Deflection y_{max} :

$$\theta = \frac{dy}{dx} = slope = 0$$

Allowable Deflection Limits

All building codes and design codes limit deflection for beam types and damage that could happen based on service condition and severity.

$$y_{max}(x) = \Delta_{actual} \leq \Delta_{allowable} = L / \text{value}$$



Use	LL only	DL+LL
Roof beams:		
Industrial	L/180	L/120
Commercial		
plaster ceiling	L/240	L/180
no plaster	L/360	L/240
Floor beams:		
Ordinary Usage	L/360	L/240
Roof or floor (damageable elements)		L/480

Beam Loads & Load Tracing

In order to determine the loads on a beam (or girder, joist, column, frame, foundation...) we can start at the top of a structure and determine the *tributary area* that a load acts over and the beam needs to support. Loads come from material weights, people, and the environment. This area is assumed to be from half the distance to the next beam over to halfway to the next beam.

The reactions must be supported by the next lower structural element *ad infinitum*, to the ground.

Design Procedure

The intent is to find the most light weight member satisfying the section modulus size.

1. Know F_b (allowable stress) for the material or F_y & F_u for LRFD.
2. Draw V & M , finding M_{max} .
3. Calculate $S_{req'd}$. This step is equivalent to determining $f_b = \frac{M_{max}}{S} \leq F_b$
4. For rectangular beams $S = \frac{bh^2}{6}$

- For steel or timber: use the section charts to find S that will work *and remember that the beam self weight will increase $S_{req'd}$* . And for steel, the design charts show the lightest section within a grouping of similar S 's. $w_{self\ wt} = \gamma A$
- For any thing else, try a nice value for b , and calculate h or the other way around.

****Determine the "updated" V_{max} and M_{max} including the beam self weight, and verify that the updated $S_{req'd}$ has been met. ****

5. Consider lateral stability
6. Evaluate horizontal shear stresses using V_{max} to determine if $f_v \leq F_v$

For rectangular beams, W 's, and others: $f_{v-max} = \frac{3V}{2A} \approx \frac{V}{A_{web}} \text{ or } \frac{VQ}{Ib}$

7. Provide adequate bearing area at supports: $f_p = \frac{P}{A} \leq F_p$

8. Evaluate shear due to torsion $f_v = \frac{T\rho}{J} \text{ or } \frac{T}{c_1ab^2} \leq F_v$

(circular section or rectangular)

9. Evaluate the deflection to determine if $\Delta_{maxLL} \leq \Delta_{LL-allowed}$ and/or $\Delta_{maxTotal} \leq \Delta_{T-allowed}$

**** note: when $\Delta_{calculated} > \Delta_{limit}$, $I_{required}$ can be found with:
and $S_{req'd}$ will be satisfied for similar self weight ****

$$I_{req'd} \geq \frac{\Delta_{too\ big}}{\Delta_{limit}} I_{trial}$$

FOR ANY EVALUATION:

Redesign (with a new section) at any point that a stress or serviceability criteria is NOT satisfied and re-evaluate each condition until it is satisfactory.

Beam Design Flow Chart

