

**ARCHITECTURAL STRUCTURES:
FORM, BEHAVIOR, AND DESIGN**

ARCH 331

DR. ANNE NICHOLS

SUMMER 2013

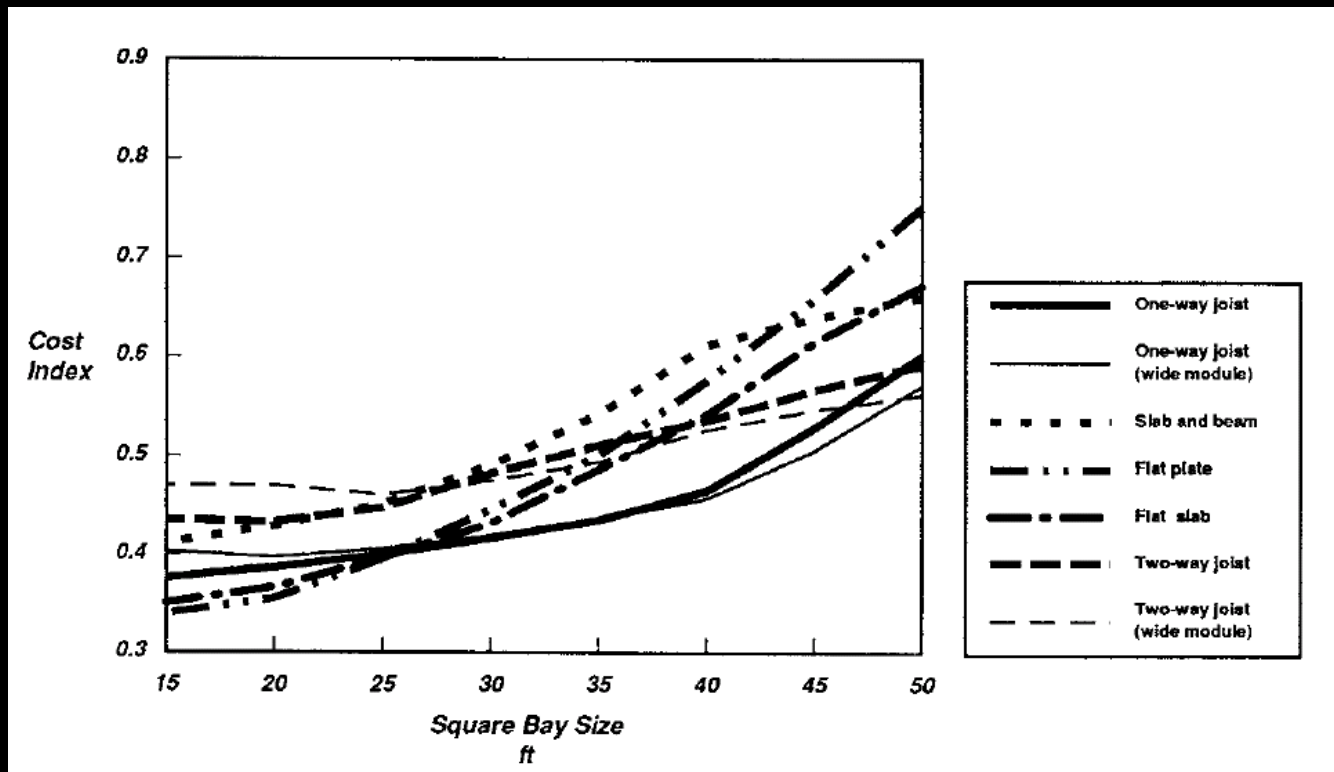
lecture
twenty two



concrete construction: <http://nisee.berkeley.edu/godden>
flat spanning systems,
columns & frames

Reinforced Concrete Design

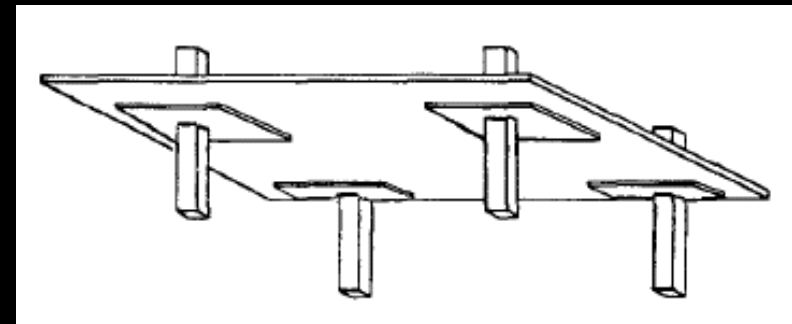
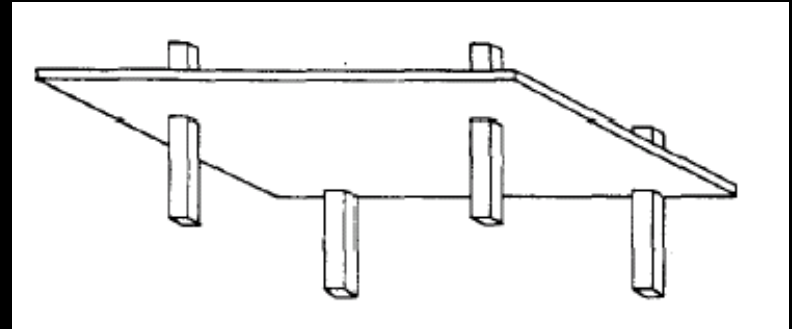
- economical & common
- resist lateral loads



Reinforced Concrete Design

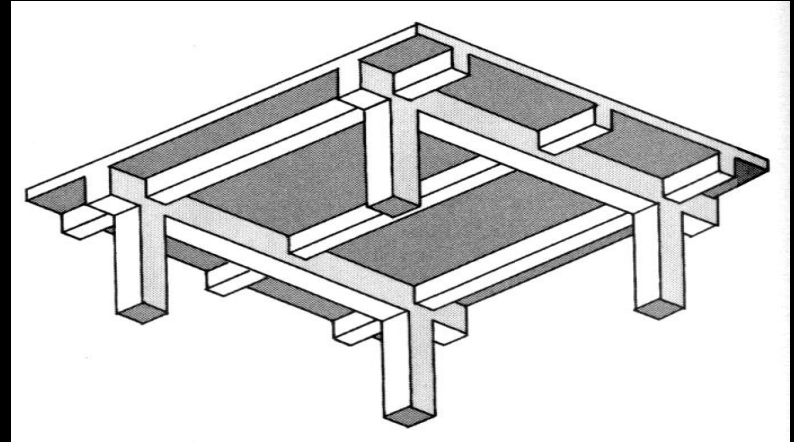
- *flat plate*
 - 5”-10” thick
 - simple formwork
 - lower story heights

- *flat slab*
 - same as plate
 - 2 ¼”–8” drop panels

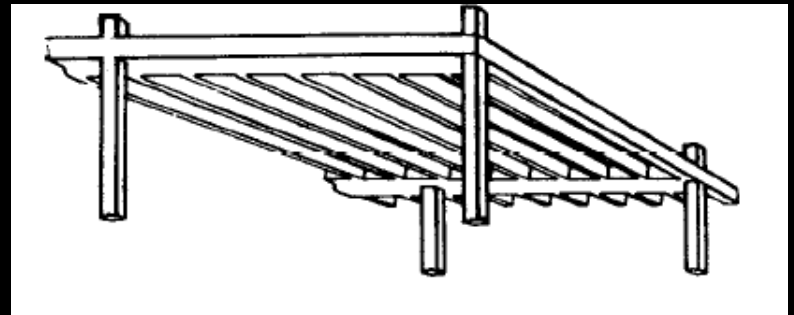


Reinforced Concrete Design

- *beam supported*
 - slab depth $\sim L/20$
 - 8"–60" deep
- *one-way joists*
 - 3"–5" slab
 - 8"–20" stems
 - 5"-7" webs

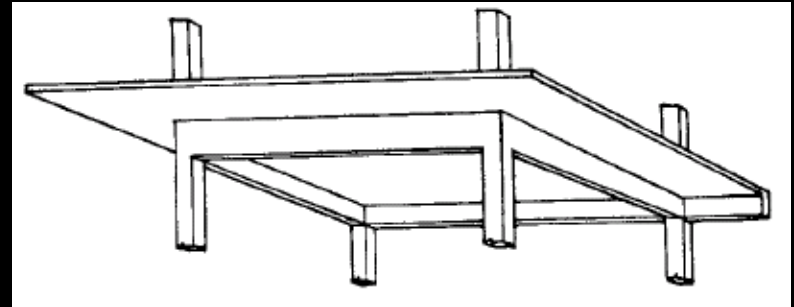
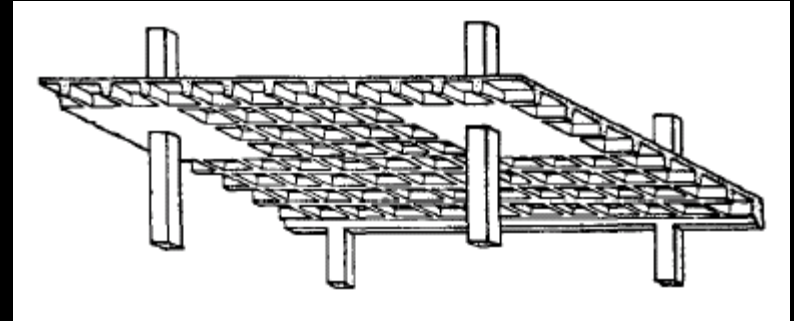


The Architect's Studio Companion



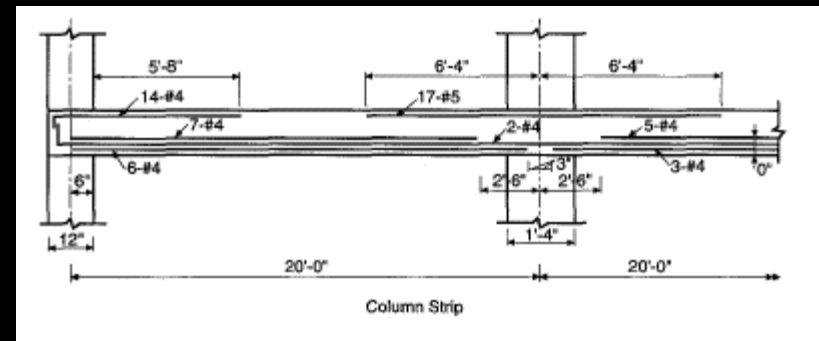
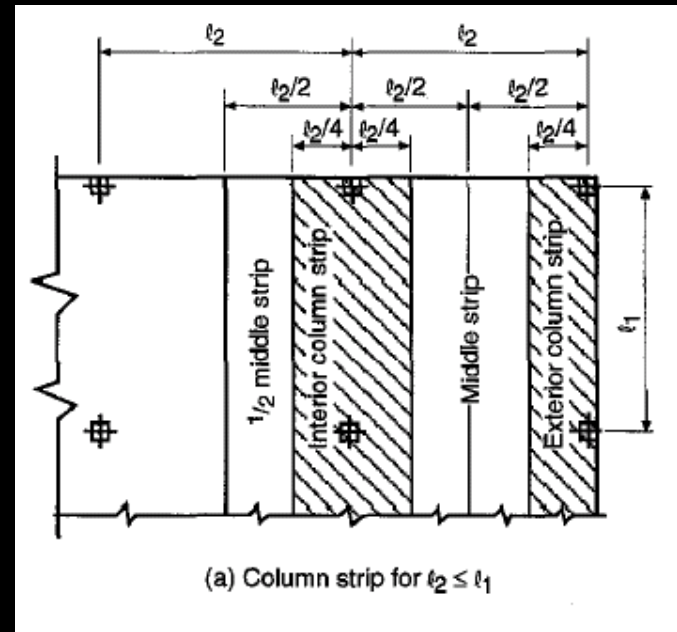
Reinforced Concrete Design

- *two-way joist*
 - “waffle slab”
 - 3”-5” slab
 - 8”-24” stems
 - 6”-8” webs
- *beam supported slab*
 - 5”-10” slabs
 - taller story heights



Reinforced Concrete Design

- *simplified frame analysis*
 - strips, like continuous beams
- *moments require flexural reinforcement*
 - top & bottom
 - both directions of slab
 - continuous, bent or discontinuous



Reinforced Concrete Design

- *one-way slabs (wide beam design)*
 - *approximate analysis for moment & shear coefficients*
 - *two or more spans*
 - *~ same lengths*
 - *w_u from combos*
 - *uniform loads with $L/D \leq 3$*
 - *l_n is clear span (+M) or average of adjacent clear spans (-M)*

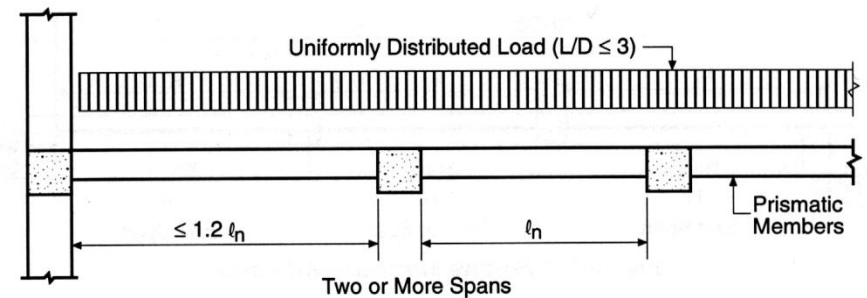


Figure 2-2 Conditions for Analysis by Coefficients (ACI 8.3.3)

Reinforced Concrete Design

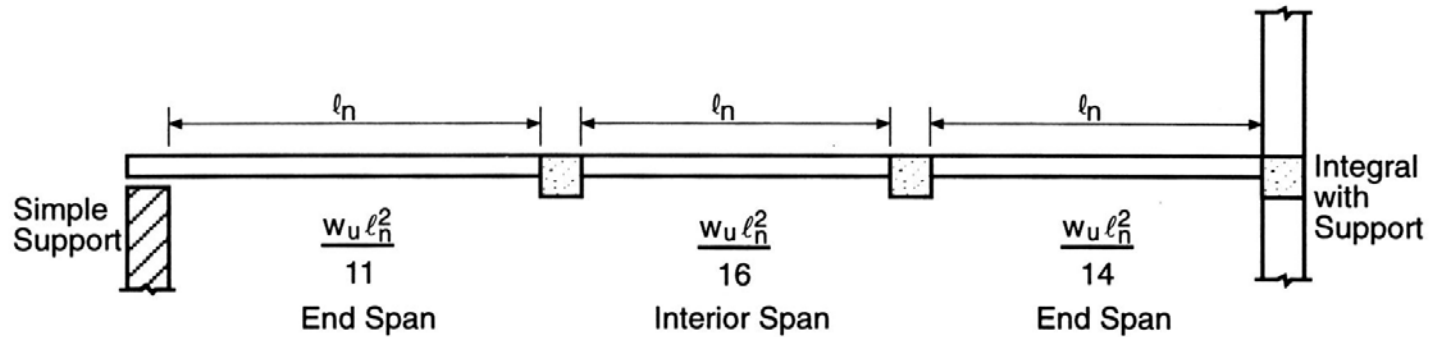


Figure 2-3 Positive Moments—All Cases

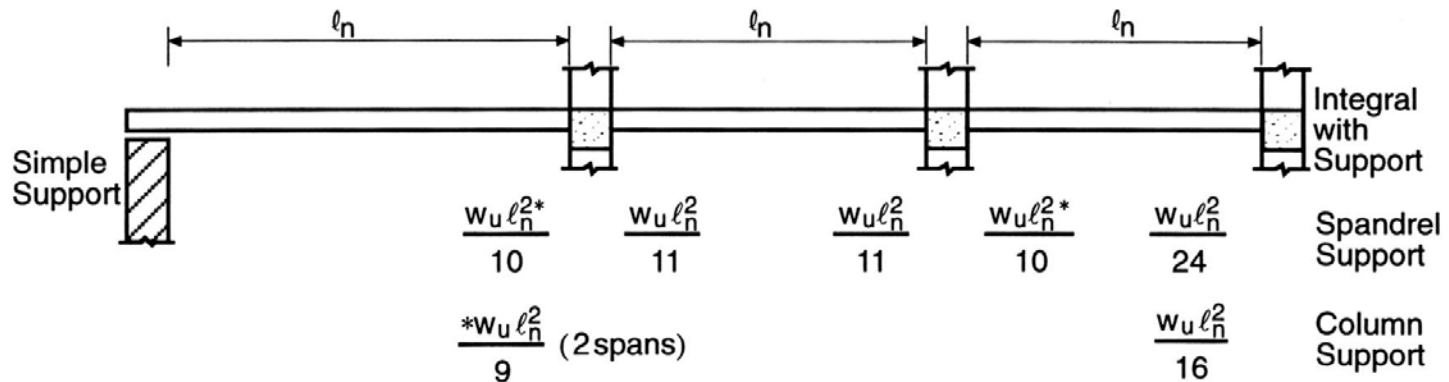
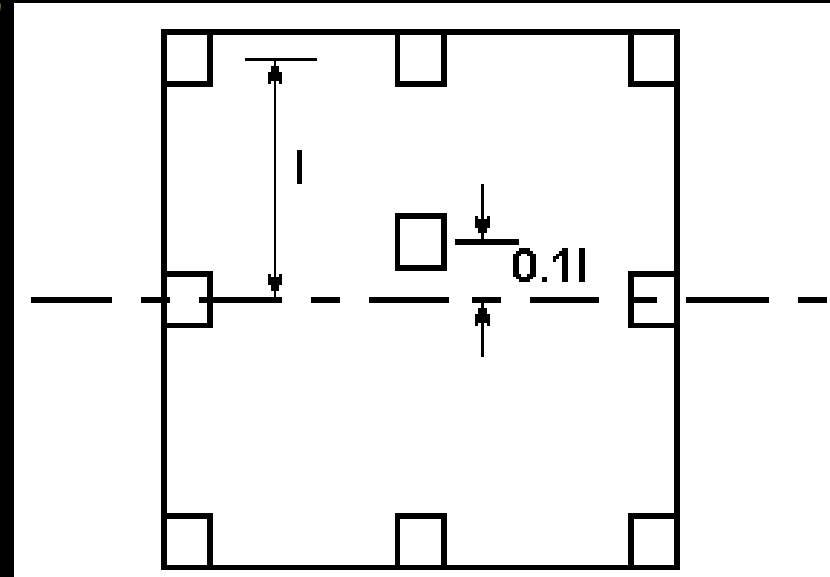


Figure 2-4 Negative Moments—Beams and Slabs

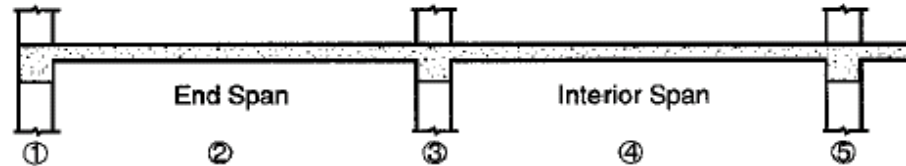
Reinforced Concrete Design

- *two-way slabs - Direct Design Method*
 - 3 or more spans each way
 - uniform loads with $L/D \leq 3$
 - rectangular panels with long/short span ≤ 2
 - successive spans can't differ $> \text{longer}/3$
 - column offset no more than 10% span



Reinforced Concrete Design

Table 4-6 Two-Way Beam-Supported Slab

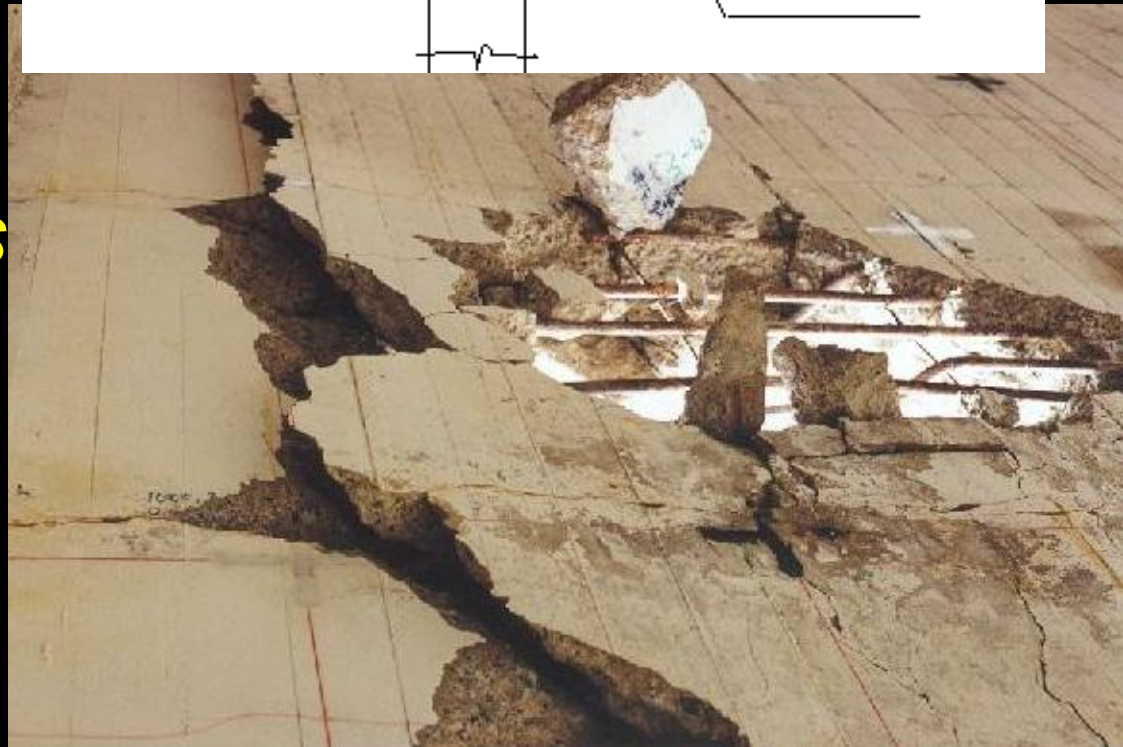
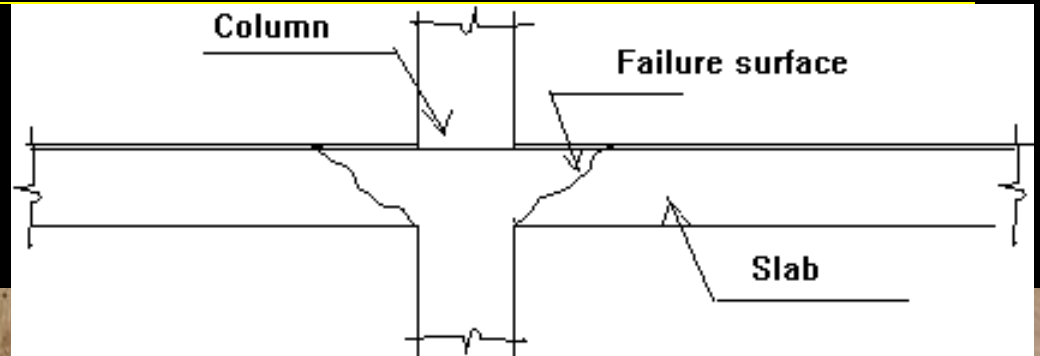


Span ratio	Slab Moments	End Span			Interior Span	
		1 Exterior Negative	2 Positive	3 First Interior Negative	4 Positive	5 Interior Negative
l_2/l_1	Total Moment	$0.16 M_o$	$0.57 M_o$	$0.70 M_o$	$0.35 M_o$	$0.65 M_o$
0.5	Column Strip	$0.12 M_o$	$0.43 M_o$	$0.54 M_o$	$0.27 M_o$	$0.50 M_o$
	Beam Slab	$0.02 M_o$	$0.08 M_o$	$0.09 M_o$	$0.05 M_o$	$0.09 M_o$
	Middle Strip	$0.02 M_o$	$0.06 M_o$	$0.07 M_o$	$0.03 M_o$	$0.06 M_o$
1.0	Column Strip	$0.10 M_o$	$0.37 M_o$	$0.45 M_o$	$0.22 M_o$	$0.42 M_o$
	Beam Slab	$0.02 M_o$	$0.06 M_o$	$0.08 M_o$	$0.04 M_o$	$0.07 M_o$
	Middle Strip	$0.04 M_o$	$0.14 M_o$	$0.17 M_o$	$0.09 M_o$	$0.16 M_o$
2.0	Column Strip	$0.06 M_o$	$0.22 M_o$	$0.27 M_o$	$0.14 M_o$	$0.25 M_o$
	Beam Slab	$0.01 M_o$	$0.04 M_o$	$0.05 M_o$	$0.02 M_o$	$0.04 M_o$
	Middle Strip	$0.09 M_o$	$0.31 M_o$	$0.38 M_o$	$0.19 M_o$	$0.36 M_o$

- Notes:
- (1) Beams and slab satisfy stiffness criteria: $\alpha_1 l_2/l_1 \geq 1.0$ and $\beta_t \geq 2.5$.
 - (2) Interpolate between values shown for different l_2/l_1 ratios.
 - (3) All negative moments are at face of support.
 - (4) Concentrated loads applied directly to beams must be accounted for separately.

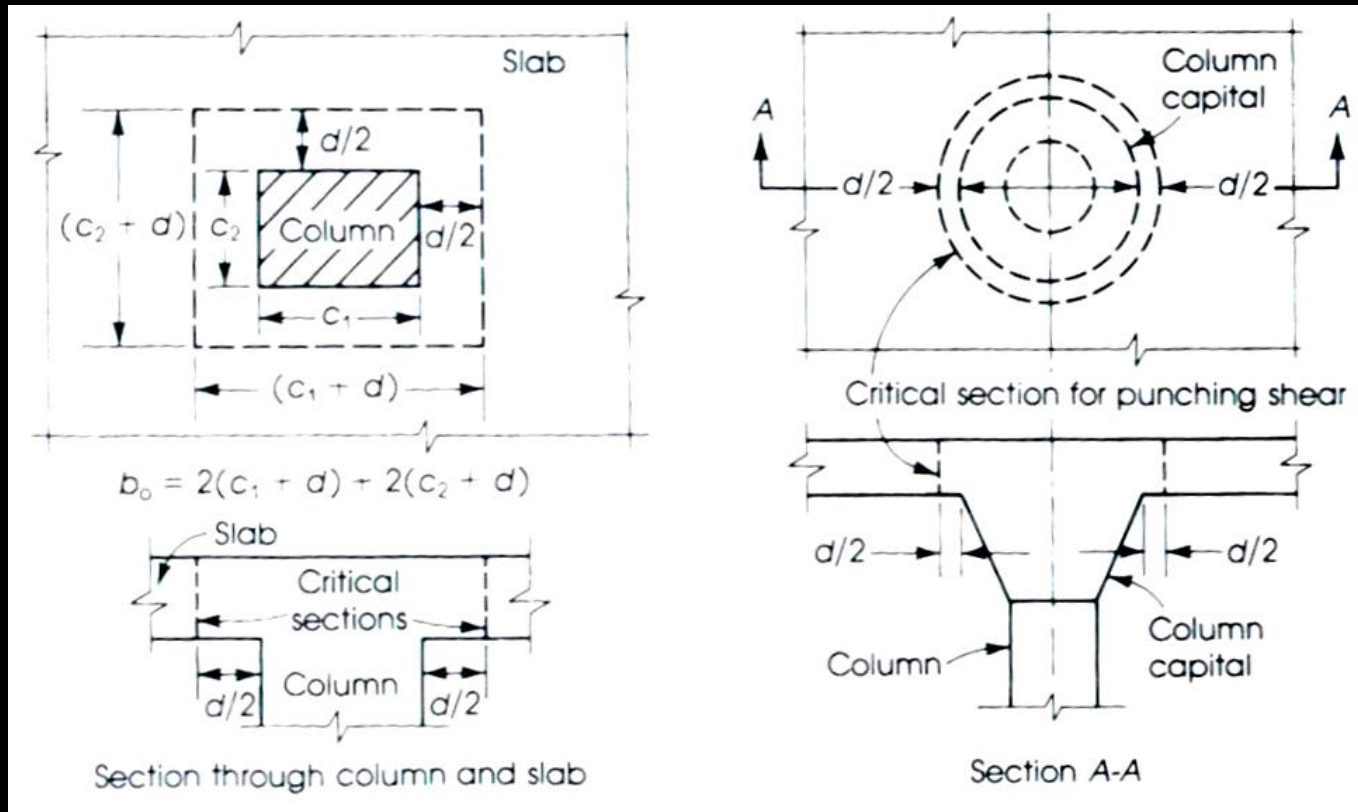
Shear in Concrete

- *at columns*
- *want to avoid stirrups*
- *can use shear studs or heads*



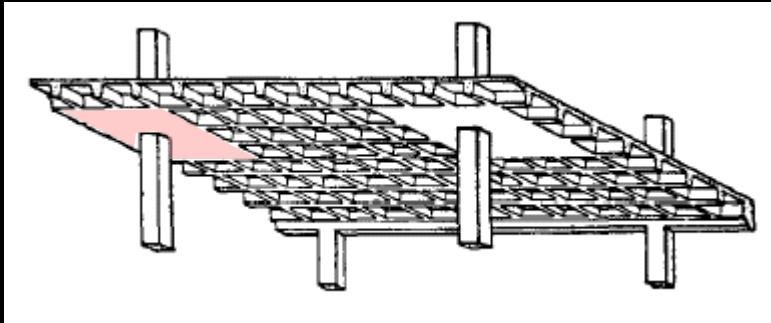
Shear in Concrete

- critical section at $d/2$ from
 - column face, column capital or drop panel



Shear in Concrete

- *at columns with waffle slabs*



Openings in Slabs

- careful placement of holes
- shear strength reduced
- bending & deflection can increase

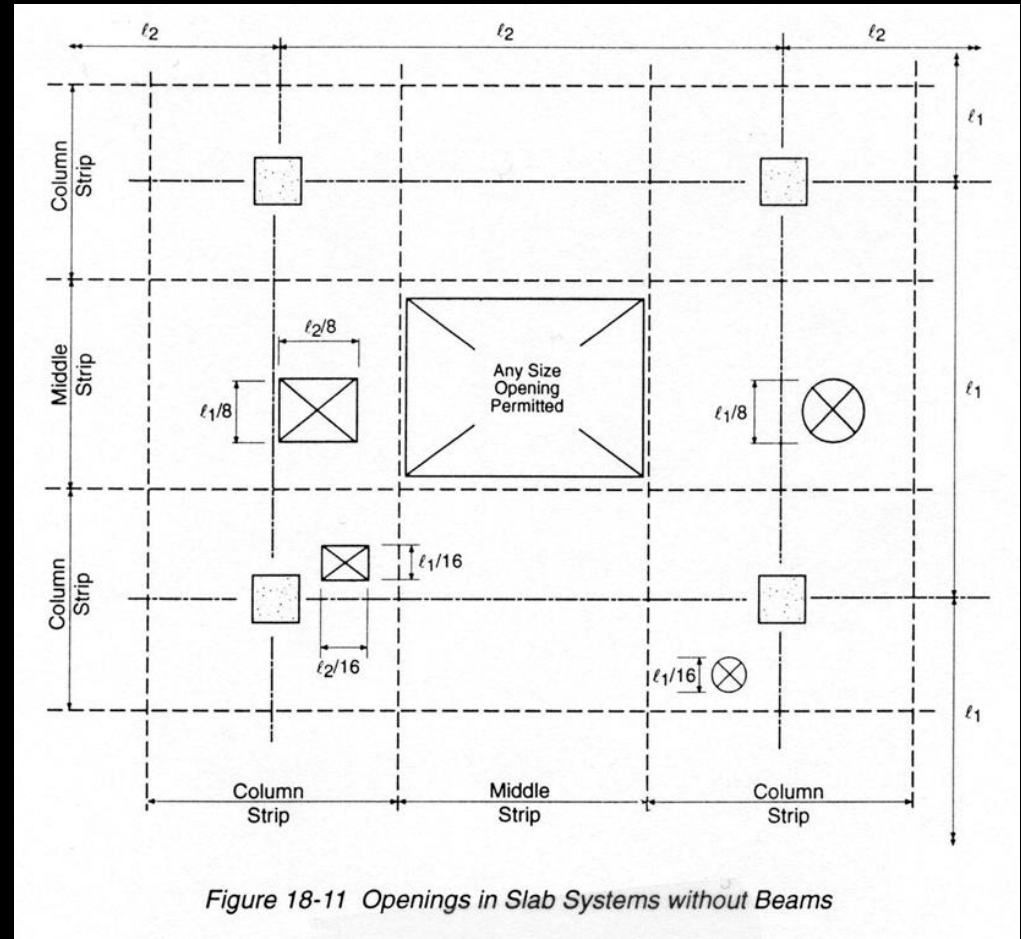
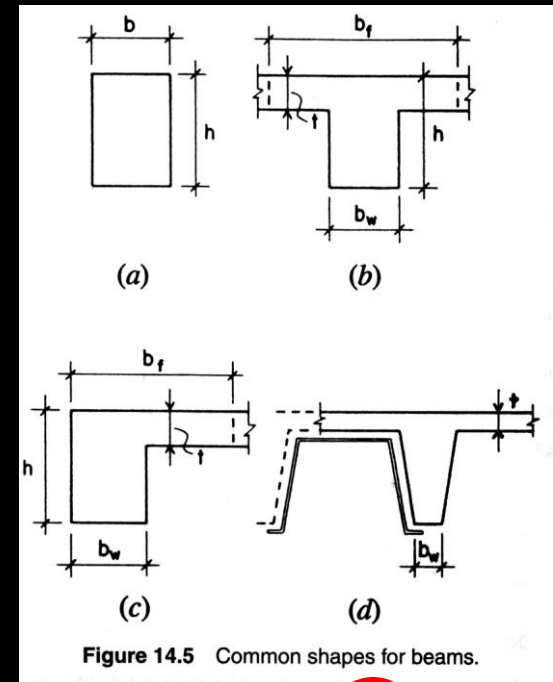


Figure 18-11 Openings in Slab Systems without Beams

General Beam Design

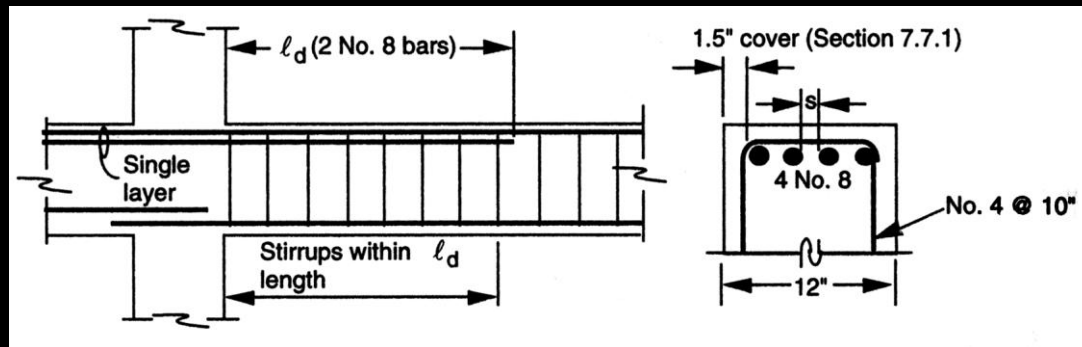
- f'_c & f_y needed
- usually size just b & h
 - even inches typical (forms)
 - similar joist to beam depth
 - $b:h$ of 1:1.5-1:2.5
 - b_w & b_f for T
 - to fit reinforcement + stirrups
- slab design, t
 - deflection control & shear



$$S = \frac{bh^2}{6}$$

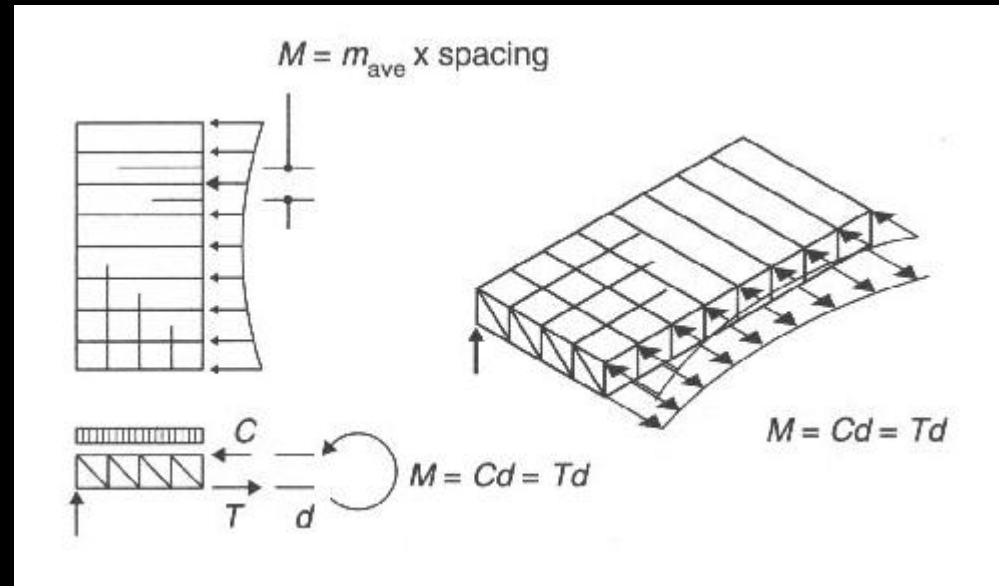
General Beam Design (cont'd)

- *custom design:*
 - *longitudinal steel*
 - *shear reinforcement*
 - *detailing*



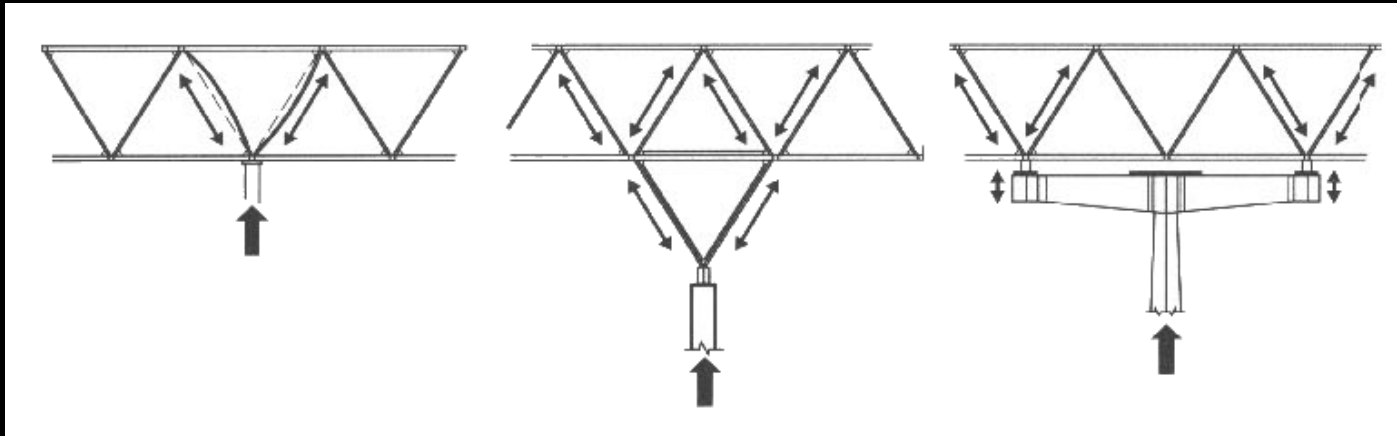
Space “Frame” Behavior

- *handle uniformly distributed loads well*
- *bending moment*
 - *tension & compression “couple” with depth*
 - *member sizes can vary, but difficult*



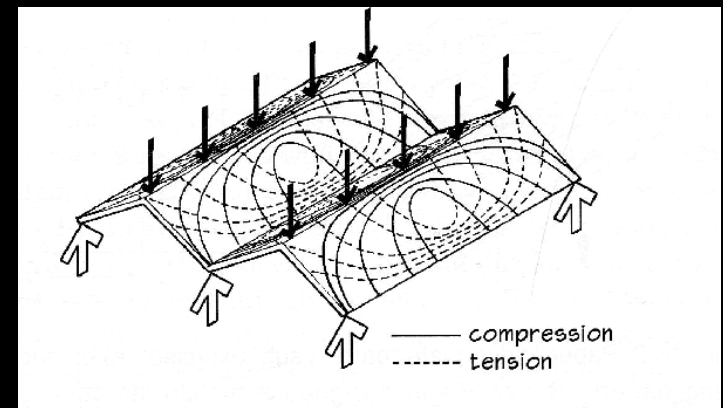
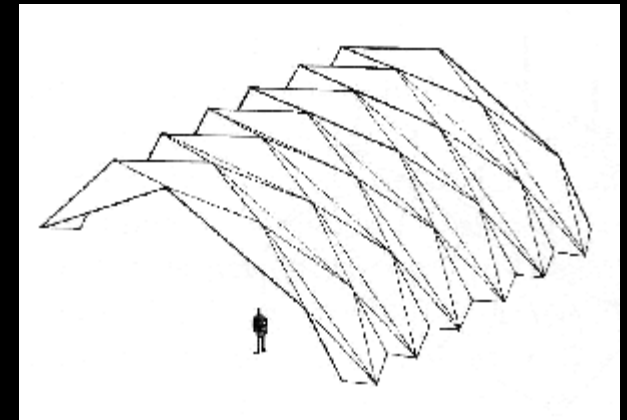
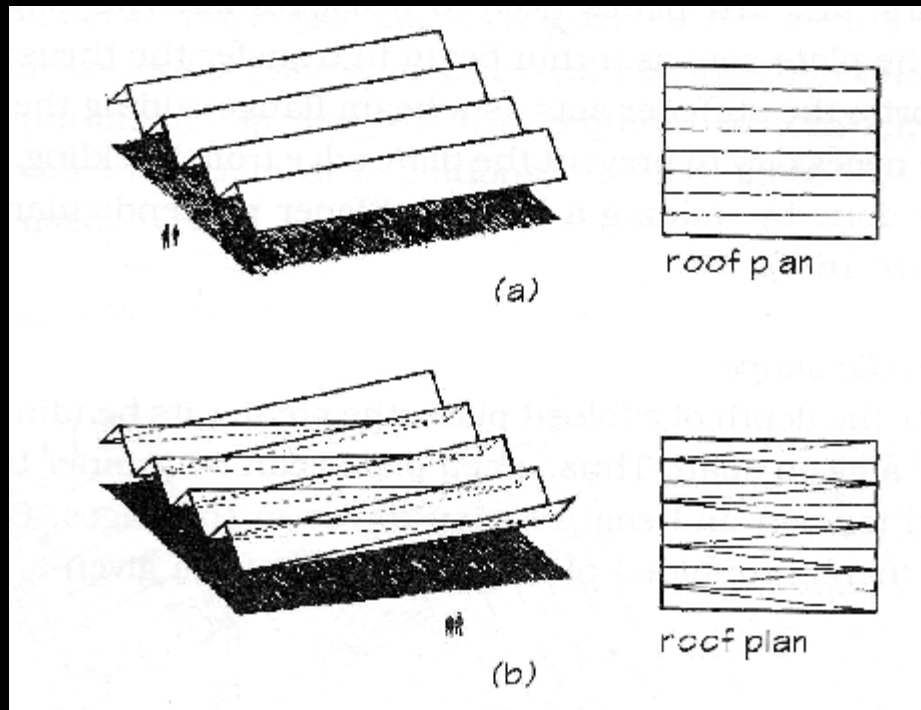
Space “Frame” Behavior

- *shear at columns*
- *support conditions still important*
 - *point supports not optimal*
- *fabrication/construction can dominate design*



Folded Plates

- *increased bending stiffness with folding*
- *lateral buckling avoided*



Folded Plates

- *common for roofs*
- *edges need stiffening*



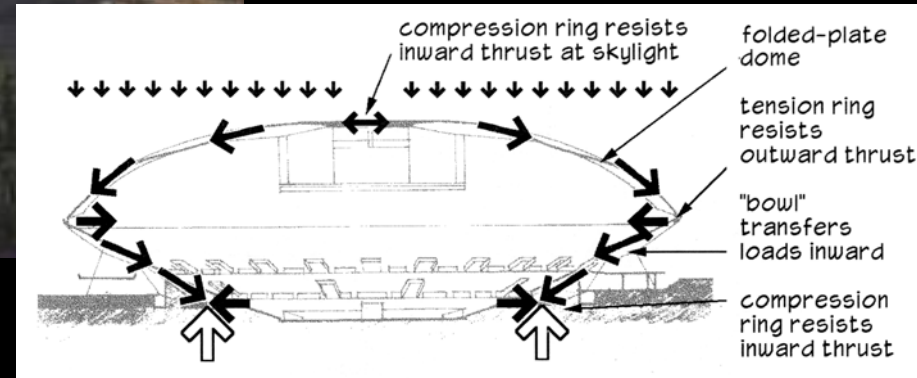
[http:// nisee.berkeley.edu/godden](http://nisee.berkeley.edu/godden)

Folded Plates



www.library.illinois.edu

- **State Farm Center (Assembly Hall), University of Illinois**
- **Harrison & Abramovitz 1963**
- **Edge-supported dome spanning 400 feet wound with 614 miles of one-fifth inch steel wire**



Concrete in Compression

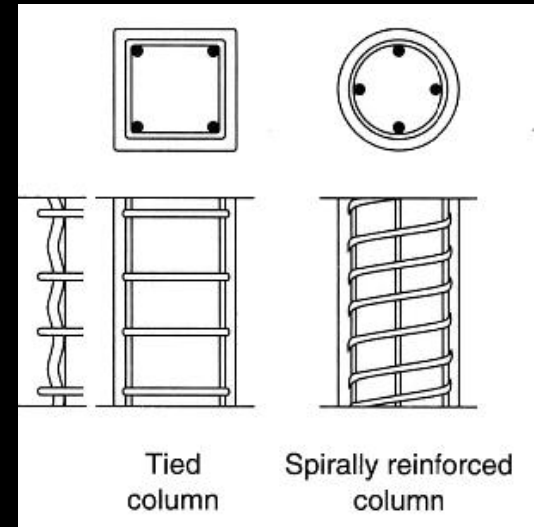
- *crushing*
- *vertical cracking*
 - *tension*
- *diagonal cracking*
 - *shear*
- f'_c



<http://www.bam.de>

Columns Reinforcement

- *columns require*
 - *ties or spiral reinforcement to “confine” concrete*
(#3 bars minimum)



- *minimum amount of longitudinal steel*
(#5 bars minimum: 4 with ties, 5 with spiral)

Slenderness

- effective length in monolithic with respect to stiffness of joint: Ψ & k
- not slender when

$$\frac{kL_u}{r} < 22$$

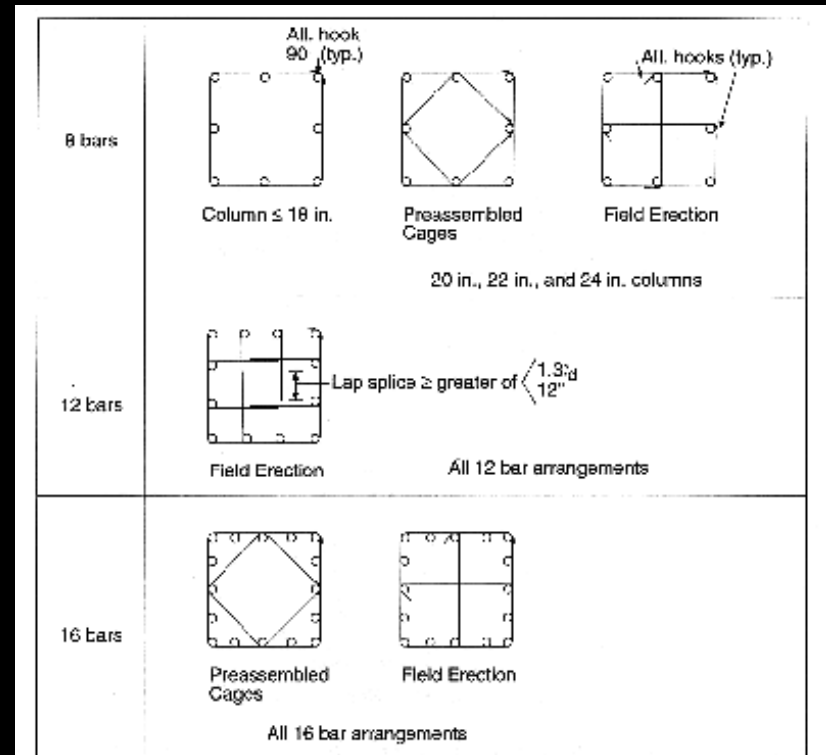
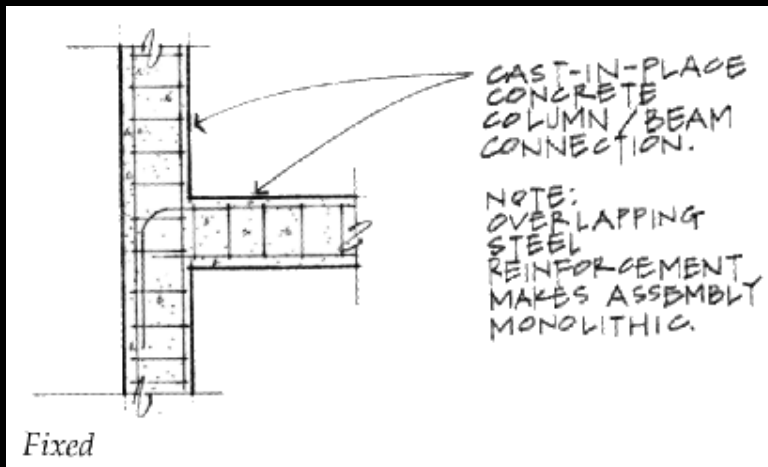
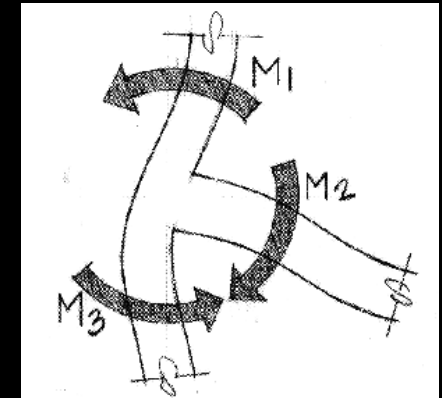
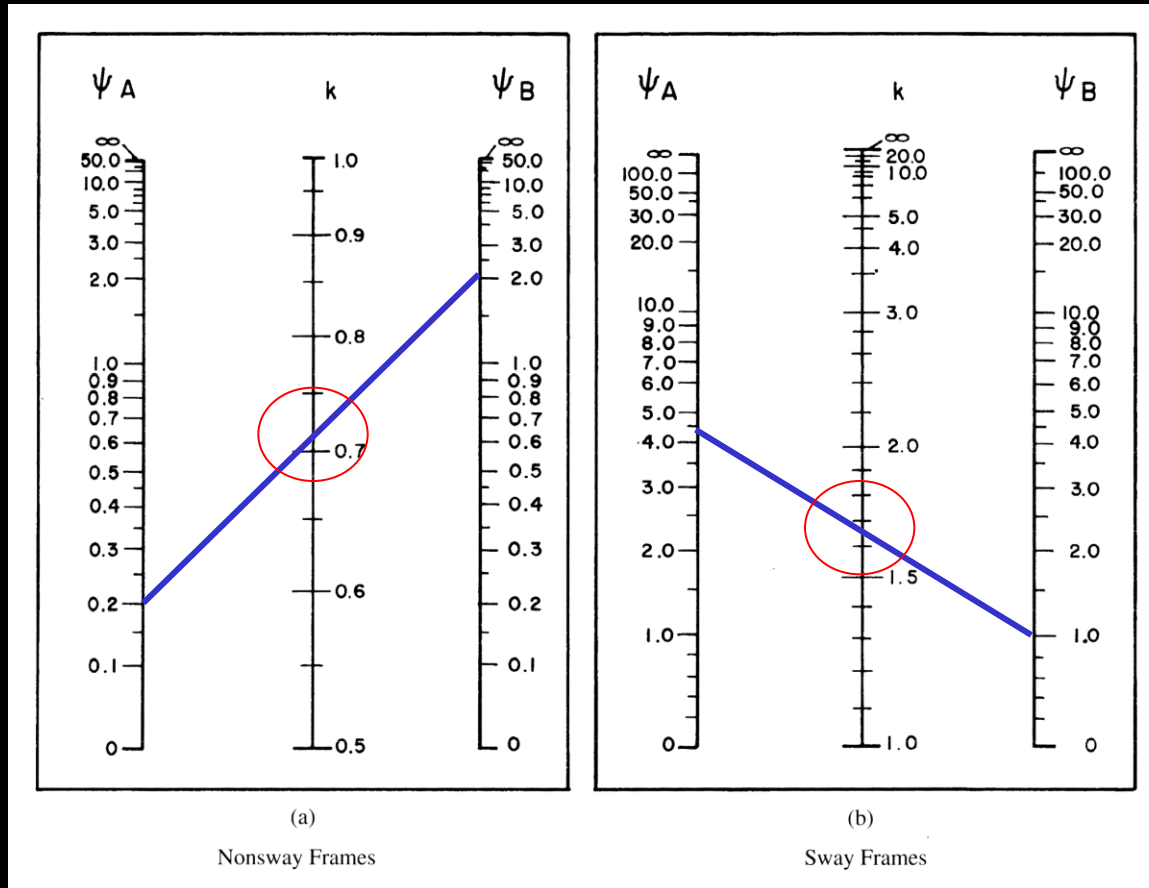


Figure 5-7 Column Tie Details

Effective Length (revisited)

- relative rotation



$$\Psi \equiv \frac{\sum EI / l_c}{\sum EI / l_b}$$

Column Behavior

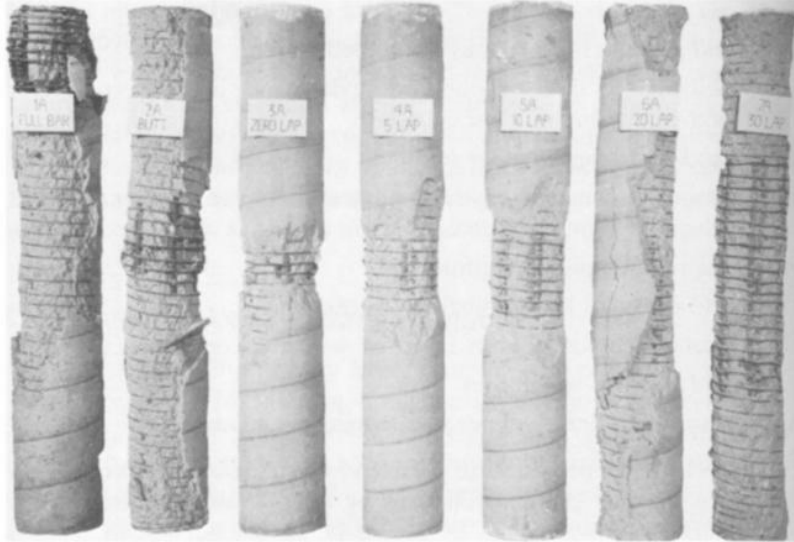


Figure 13.3.2 Spirally reinforced column behavior. (Courtesy of Portland Cement Association.)

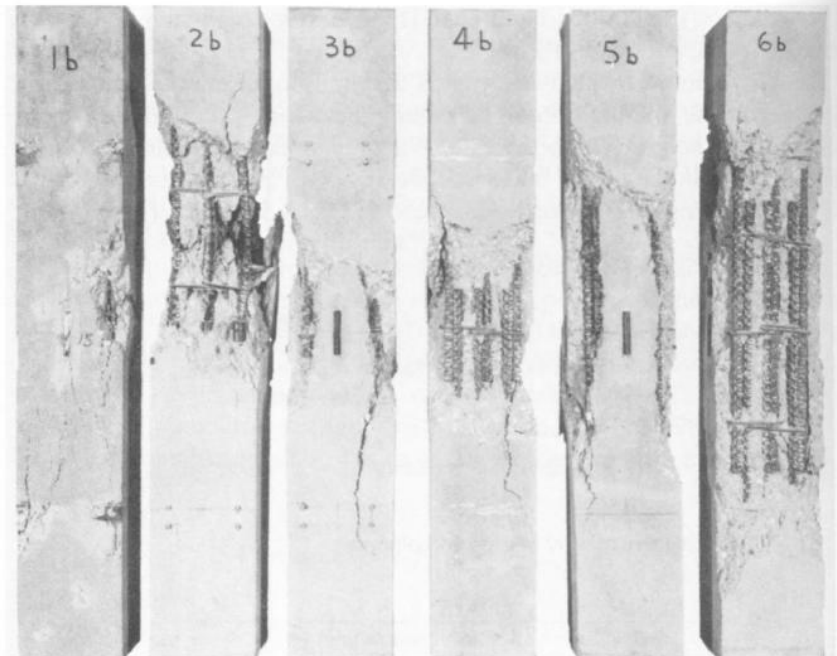


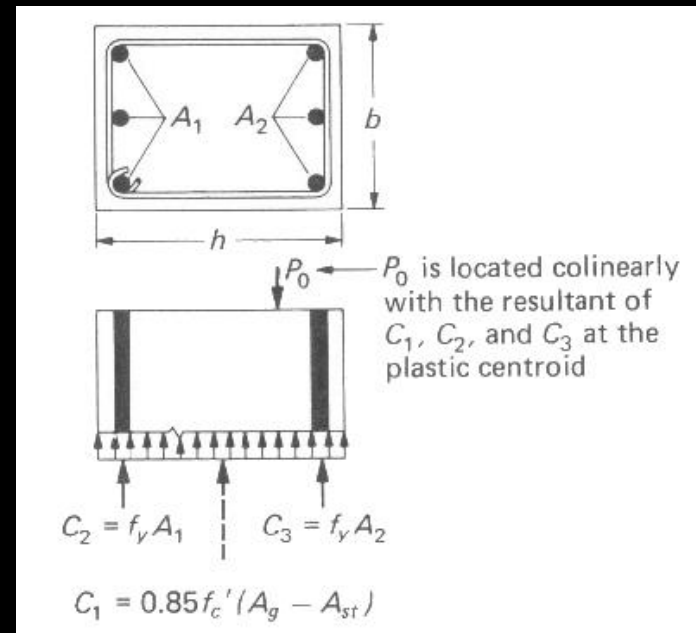
Figure 13.3.3 Tied column behavior. (Courtesy of Portland Cement Association.)

Column Design

- $\phi_c = 0.65$ for ties, $\phi_c = 0.75$ for spirals
- P_o – no bending

$$P_o = 0.85 f'_c (A_g - A_{st}) + f_y A_{st}$$

- $P_u \leq \phi_c P_n$
 - ties: $P_n = 0.8 P_o$
 - spiral: $P_n = 0.85 P_o$
- **nominal axial capacity:**
 - presumes steel yields
 - concrete at ultimate stress



Columns with Bending

- *eccentric loads can cause moments*
- *moments can change shape and induce more deflection*
($P-\Delta$)

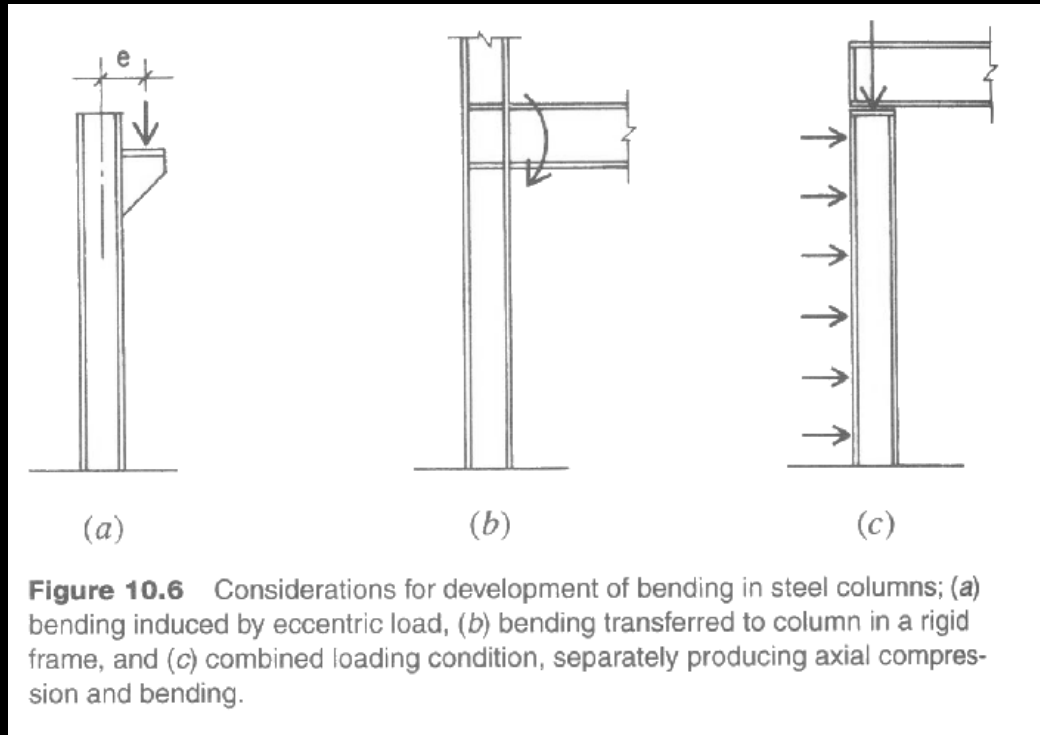
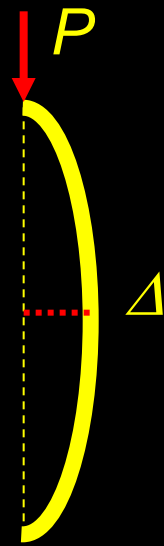


Figure 10.6 Considerations for development of bending in steel columns; (a) bending induced by eccentric load, (b) bending transferred to column in a rigid frame, and (c) combined loading condition, separately producing axial compression and bending.

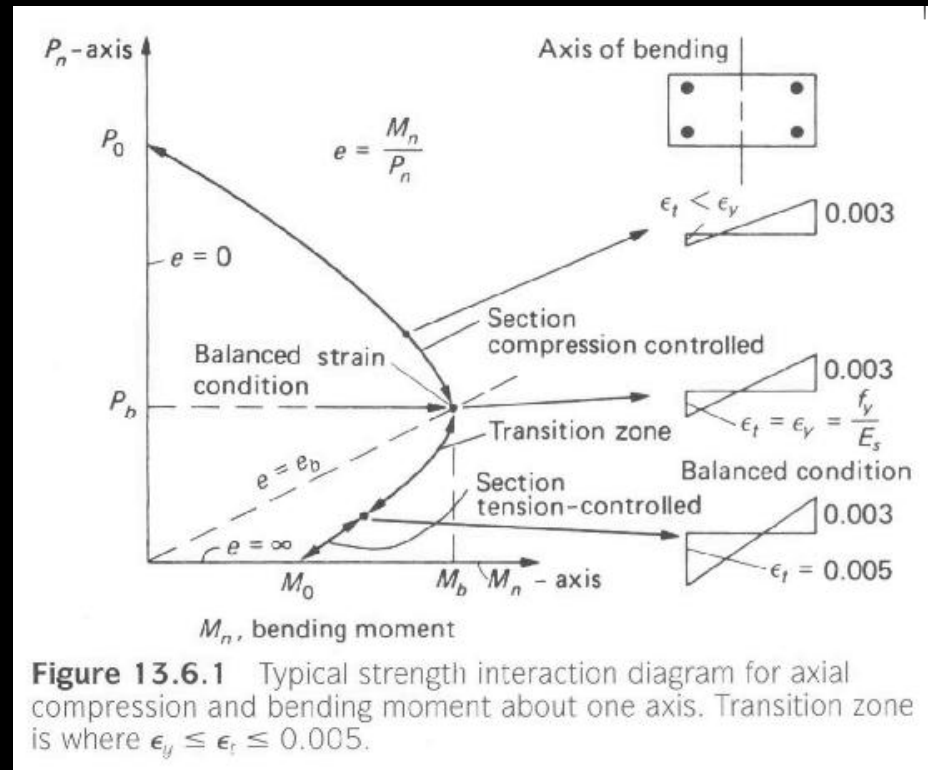
Columns with Bending

- for ultimate strength behavior, ultimate strains can't be exceeded

- concrete 0.003

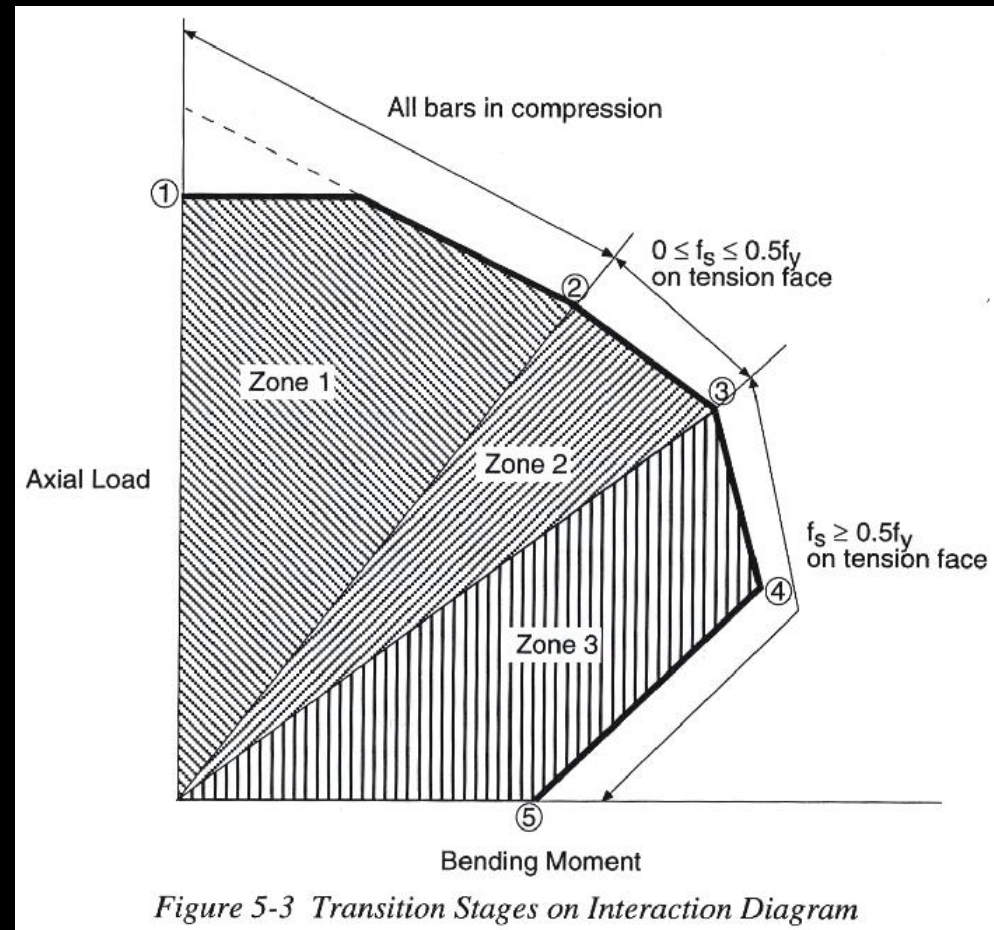
- steel $\frac{f_y}{E_s}$

- P reduces with M



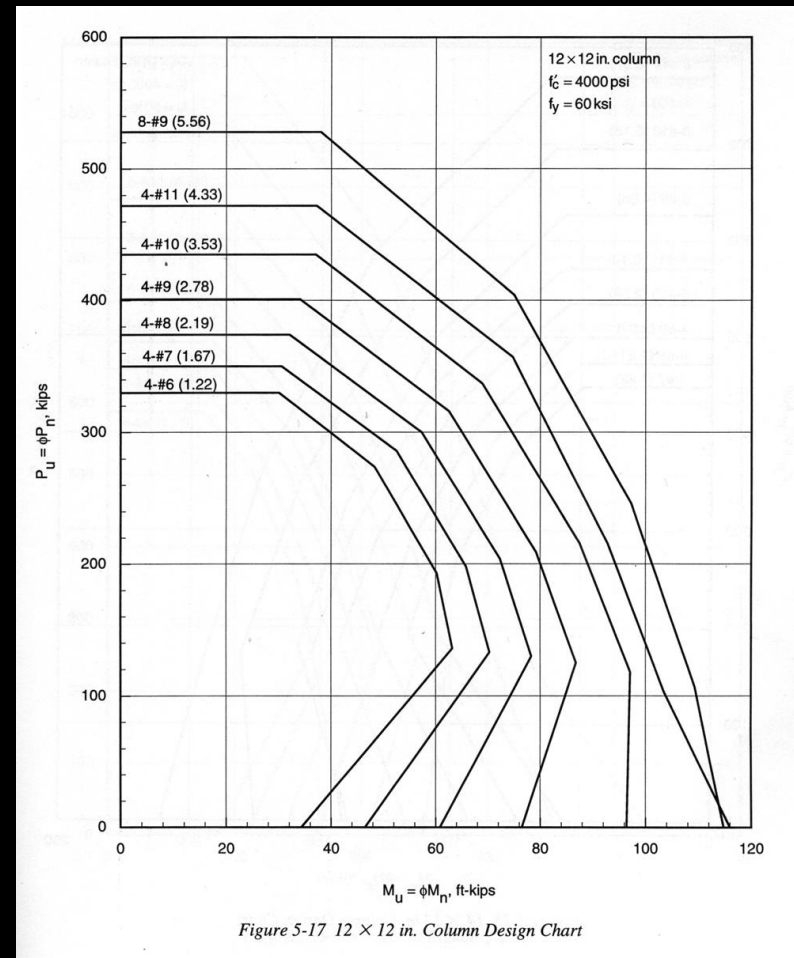
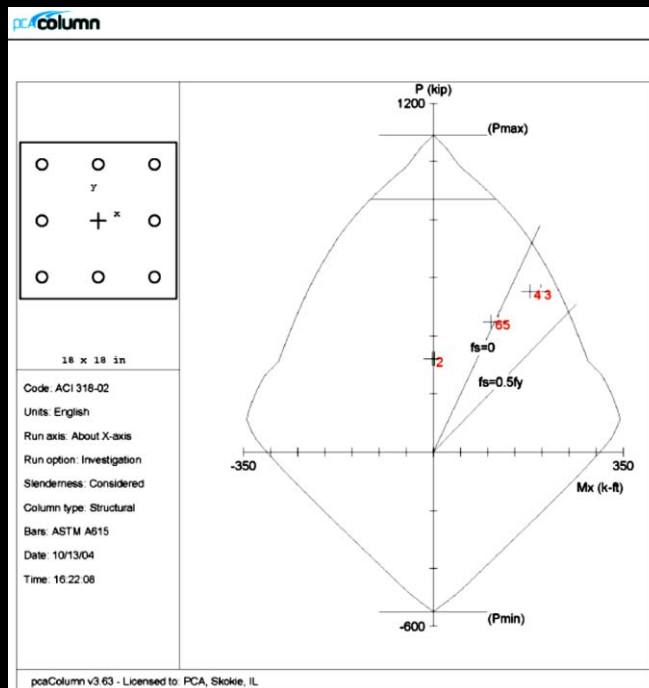
Columns with Bending

- need to consider combined stresses
- linear strain
- steel stress at or below f_y
- plot interaction diagram



Design Methods

- calculation intensive
 - handbook charts
 - computer programs



Design Considerations

- *bending at both ends*
 - $P-\Delta$ maximum
- *biaxial bending*
- *walls*
 - *unit wide columns*
 - “*deep*” beam shear
- *detailing*
 - *shorter development lengths*
 - *dowels to footings*

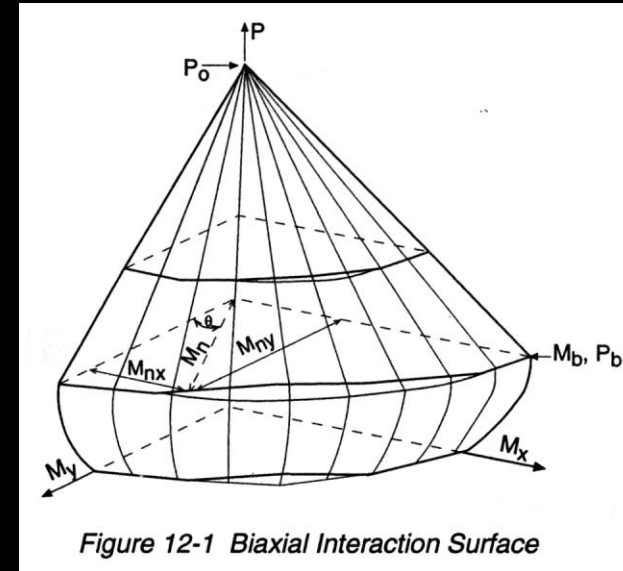
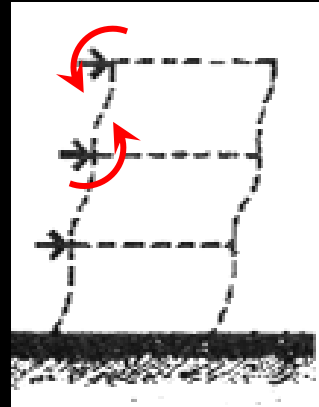
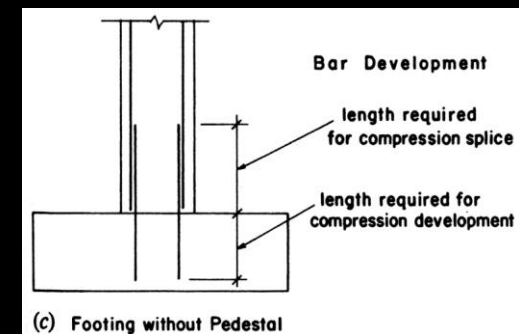


Figure 12-1 Biaxial Interaction Surface



(c) Footing without Pedestal