ARCH 331: Practice Quiz 6

Note: No aids are allowed for part 1. One side of a letter sized paper with notes is allowed during part 2, along with a silent, non-programmable calculator. There are reference charts for part 2, shown on pages 2-3.

Clearly show your work and answer.

Part 1) Worth 5 points (conceptual questions)

Part 2) Worth 45 points

(NOTE: The member size, load magnitudes, reinforcement, and materials can and will be changed for the quiz! The beam supports will not change.)

A 28 ft simply supported reinforced concrete beam (shown) is 14 in. wide by 22 in. deep with 10-#8 bars (two layers). The effective depth, d = 17.625 in.. It has 3000 psi concrete and Grade 40 reinforcement ($f_v = 40 \text{ ksi}$). The beam has a total factored distributed load of 3000 lb/ft. There will be #3 U stirrups.

- a) Determine if the beam is adequate for flexure and reinforcing requirements when $M_u = 294$ k-ft.
- b) Determine the key values for shear, and determine the lengths over which the beam requires stirrups for strength and stirrups for crack control. $V_{u-max} = 42 \text{ k}$.
- c) Determine the spacing required for strength with the maximum design shear.

A 9 in. thick solid one-way continuous slab (no figure) with a 12 ft span is to be designed for a maximum factored moment of 19 k-ft/ft of width. It has 3000 psi concrete and Grade 60 reinforcement $(f_v = 60 \text{ ksi})$. Assume d = 8 in.

- d) Determine the required reinforcement and spacing in both directions. (Note: checking moment capacity adequacy is not required for this part.)
- e) Find the minimum thickness if deflections will not be computed.

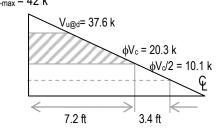
b = 14 in22

10 - #8 bars

Answers - Not provided on actual quiz!

- $\frac{\text{defined quiz!}}{\phi M_n = 313 \text{ k-ft} > M_u \ \rho_{min} < 0.032} \not \leq \rho_{max} \ \text{... Not Oknstakingly researched.}$ $V_{u@d} = 37.6 \text{ k, } \phi V_c = 20.3 \text{ k, } \frac{1}{2} \phi V_c = 10.1 \text{ keeps the proof of the pr$
- c) $s_{req'd} = 6.72$ in (and less than d/2)
- d) $R_n \approx 330 \text{ psi}$, $\rho \approx 0.007$, $A_{\text{smin-temp}} = 0.194 \text{ in}_2/\text{ft.}$; one possibility is #4 at 3.5 in.

e) t = 6.0 in.



110

10

 $f_c' = 6000 \ \frac{100}{f_y}$

6

90

ω

 $f_c' = 5000_$ $f_y = 40,000_-$

8

70

 $f_c' = 4000$ $f_y = 40,000$

> $f_c' = 4000$ $f_y = 60,000$

1000

= 50,000

0

b

0.05

0.04

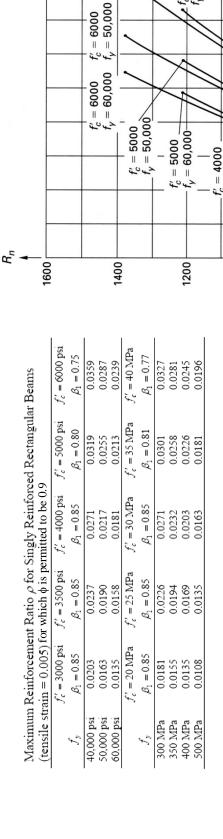
0.03

0.02

0.0

Min p controls

REFERENCE CHARTS FOR QUIZ 6



STEEL REINFORCEMENT INFORMATION

R_n, MPa

_В», кдf/ст²

2

20

; = 3000 ; = 40,000_

 $f_c' = 3000$ $f_{\gamma} = 60,000$

800

Coefficient of resistance, R_n, psi

3

30

400

20

 $= R_n b d^2$

N

200

10

40

 $f_c' = 3000$ $f_{\gamma} = 50,000$

009

9

9

Table 3.7.1

Total Areas for Various Numbers of Reinforcing Bars

9	Nominal	Waight					Numpe	Number of Bar	rs.			
Size	Diameter (in.)	(lb/ft)	-	2	3	4	5	9	7	∞	6	
#3	0.375	0.376	0.11	0.22	0.33	0.4	0.55	99.0	0.77	0.88	0.99	_
#4	0.500	0.668	0.20	0.40	0.60	0.80	1.00	1.20	1.40	1.60	1.80	N
#2	0.625	1.043	0.31	0.62	0.93	1.24	1.55	1.86	2.17	2.48	2.79	e
9#	0.750	1.502	0.44	0.88	1.32	1.76	2.20	2.64	3.08	3.52	3.96	4
#1	0.875	2.044	09.0	1.20	1.80	2.40	3.00	3.60	4.20	4.80	5.40	9
**	1.000	2.670	0.79	1.58	2.37	3.16	3.95	4.74	5.53	6.32	7.11	-
6#	1.128	3.400	1.00	2.00	3.00	4.00	5.00	9009	7.00	8.00	9.00	2
#10	1.270	4.303	1.27	2.54	3.81	5.08	6.35	7.62	8.89	10.16	11.43	7
#	1.410	5.313	1.56	3.12	4.68	6.24	7.80	9.36	10.92	12.48	14.04	15
#14	1.693	7.65	2.25	4.50	6.75	9.00	11.25	13.50	15.75	18.00	20.25	22
#18°	2.257	13.60	4.00	8.00	12.00	16.00	20.00	24.00	28.00	32.00	36.00	4

^{* #14} and #18 bars are used primarily as column reinforcement and are rarely used in beams.

Figure 3.8.1 Strength curves $(R_n \text{ vs } \rho)$ for singly reinforced rectangular sections. Upper limit of curves is at ρ_{\max} (tensile strain of 0.004)

Reinforcement ratio, ρ

REFERENCE CHARTS FOR QUIZ 6

Table 3-8 ACI Provisions for Shear Design*

$V_{\mathbf{u}} > \Phi V_{\mathbf{c}}$	$\frac{p^{t}y\phi}{s(^{\circ})\Lambda\phi - ^{n}\Lambda)}$	$\frac{\phi A_{v} t_{y} d}{V_{u} - \phi V_{c}}$	4 in.	$\frac{d}{2}$ or 24 in, for $\left(V_{u} - \phi V_{c}\right) \le \phi 4 \sqrt{\xi}$ $b_{w}d$	$\frac{d}{4} \text{ or } 12 \text{ in. for } \left(V_{\text{u}} - \phi V_{\text{c}} \right) > \phi 4 \sqrt{f_{\text{c}}} \text{ bwd}$
$\phi V_c \ge V_u > \frac{\phi V_c}{2}$	^k ł s ^w 905	A _v f _y 50b _w		d or 24 in.	
$V_{\rm U} \le \frac{\Phi V_{\rm C}}{2}$	none	_	_	-	
	tirrups, Av	Required	Recommended Minimum [†]	‡	Maximum ¹ 1 (ACI 11.5.4)
	** Required area of stirrups, A _V			Stirrup spacing, s	

*Members subjected to shear and flexure only; $\phi V_c = \phi 2 \sqrt{f_c^c} \, b_w d$, $\phi = 0.75$ (ACI 11.3.1.1) **A $_v = 2 \times Ab_v$ for U stirrups; $f_y \le 60$ ksi (ACI 11.5.2) †*A practical limit for minimum spacing is d/4 †*HMaximum spacing based on minimum shear reinforcement (= A $_v f_y \le 0b_w$) must also be considered

(ACI 11.5.5.3).

TABLE 13.6 Areas Provided By Spaced Reinforcement

Spacing			DIC.			יוים דו היותכת (יווי עד עומון)			
(in.)	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	No. 9	No. 10	No. 1
3	0.44	08.0	1.24	1.76	2.40	3.16	4.00		
3.5	0.38	69.0	1.06	1.51	2.06	2.71	3.43	4.35	
4	0.33	09.0	0.93	1.32	1.80	2.37	3.00	3.81	4.68
4.5	0.29	0.53	0.83	1.17	1.60	2.11	2.67	3.39	4.16
2	0.26	0.48	0.74	1.06	4.1	1.89	2.40	3.05	3.74
5.5	0.24	0.44	89.0	96.0	1.31	1.72	2.18	2.77	3.40
9	0.22	0.40	0.62	0.88	1.20	1.58	2.00	2.54	3.12
7	0.19	0.34	0.53	0.75	1.03	1.35	1.71	2.18	2.67
∞	0.16	0.30	0.46	99.0	0.00	1.18	1.50	1.90	2.34
6	0.15	0.27	0.41	0.59	0.80	1.05	1.33	1.69	2.08
10	0.13	0.24	0.37	0.53	0.72	0.95	1.20	1.52	1.87
=	0.12	0.22	0.34	0.48	0.65	98.0	1.09	1.38	1.70
12	0.11	0.20	0.31	0.44	0.60	0.79	1.00	1.27	1.56
13	0.10	0.18	0.29	0.40	0.55	0.73	0.92	1.17	4.1
14	0.00	0.17	0.27	0.38	0.51	89.0	98.0	1.09	1.34
15	0.00	0.16	0.25	0.35	0.48	0.63	0.80	1.01	1.25
91	0.08	0.15	0.23	0.33	0.45	0.59	0.75	0.95	1.17
18	0.07	0.13	0.21	0.29	0.40	0.53	0.67	0.85	1.04
24	0.05	0.10	0.15	0.22	0.30	0.39	0.50	0.63	0.78

and and		Minimum th	Minimum thickness, h	
	Simply sup- ported	One end continuous	Both ends continuous	Cantilever
Member	Members no other construdeflections.	Members not supporting or attached to partitions or other construction likely to be damaged by large deflections.	or attached to be damaged	partitions o by large
Solid one- way slabs	6/20	6/24	6/28	6/10
Beams or ribbed one- way slabs	6/16	6/18.5	6/21	8/7

Notes: 1) Span length ℓ is in inches. 2) Values given shall be used directly for members with normalweight concrete ($\mathbf{w}_{c} = 145 \, \mathrm{lb} 1t^{2}$) and Grade 60 reinforcement. For other conditions, the values shall be modified as follows: a for structural lightweight concrete having unit weight in the range 90-120 lb/ft², the values shall be multiplied by ($\mathbf{1.65} = \mathbf{0.005} \mathbf{w}_{c}$) but not less than 1.09, where \mathbf{w}_{c} is the unit weight in lb/ft². b) For \mathbf{f}_{y} other than 60,000 psi, the values shall be multiplied by ($\mathbf{0.44} + \mathbf{f}_{y}/\mathbf{100,000}$).