## Moments of Inertia

## Notation:

| A | = name for area | $r_{o}$ | polar radius of gyration |
| :---: | :---: | :---: | :---: |
| $b$ | = name for a (base) width | $r_{x}$ | $=$ radius of gyration with respect to an |
| $d$ | $\begin{aligned} & =\text { calculus symbol for differentiation } \\ & =\text { name for a difference } \\ & =\text { name for a depth } \end{aligned}$ | $r_{y}$ |  |
| $d_{x}$ | $=$ difference in the x direction | $t_{f}$ | $=$ thickness of a flange |
|  | etween an area centroid ( $\overline{\mathrm{x}}$ ) and | $t_{w}$ | $=$ thickness of web of wide flange |
|  | the centroid of the composite shape | $x$ | = horizontal distance |
|  | ( $\hat{\mathrm{x}}$ ) | $\bar{x}$ | $=$ the distance in the x direction from |
| $d_{y}$ | $=$ difference in the y direction between an area centroid ( $\overline{\mathrm{y}}$ ) and the centroid of the composite shape ( $\hat{\mathrm{y}}$ ) | $\hat{x}$ | a reference axis to the centroid of a shape <br> $=$ the distance in the x direction from <br> a reference axis to the centroid of a |
| $h$ | $=$ name for a height |  | composite shape |
| I | $=$ moment of inertia about the centroid | ${ }^{\prime} \bar{y}$ | = vertical distance <br> $=$ the distance in the $y$ direction from |
| $I_{c}$ | $=$ moment of inertia about the centroid |  | a reference axis to the centroid of a shape |
| $I_{x}$ | $\begin{aligned} & =\text { moment of inertia with respect to an } \\ & x \text {-axis } \end{aligned}$ | $\hat{y}$ | $=$ the distance in the y direction from a reference axis to the centroid of a |
| $I_{y}$ | $\begin{aligned} & =\text { moment of inertia with respect to a } \\ & y \text {-axis } \end{aligned}$ | L | composite shape <br> = plate symbol |
| $J_{o}$ | $=$ polar moment of inertia, as is $J$ | I | = symbol for integration |
| O | $=$ name for reference origin | $\Sigma$ | umation symbol |

- The cross section shape and how it resists bending and twisting is important to understanding beam and column behavior.
- Definition: Moment of Inertia; the second area moment

$$
I_{y}=\int x^{2} d A \quad I_{x}=\int y^{2} d A
$$

We can define a single integral using a narrow strip:
for $I_{x}$, strip is parallel to $x \quad$ for $I_{y}$, strip is parallel to $y$

*I can be negative if the area is negative (a hole or subtraction).

- A shape that has area at a greater distance away from an axis through its centroid will have a larger value of I.

- Just like for center of gravity of an area, the moment of inertia can be determined with respect to any reference axis.
- Definition: Polar Moment of Inertia; the second area moment using polar coordinate axes

$$
\begin{aligned}
& J_{o}=\int r^{2} d A=\int x^{2} d A+\int y^{2} d A \\
& J_{o}=I_{x}+I_{y}
\end{aligned}
$$

- Definition: Radius of Gyration; the distance from the moment of inertia axis for an area at which the entire area could be considered as being concentrated at.

$I_{x}=r_{x}^{2} A \Rightarrow r_{x}=\sqrt{\frac{I_{x}}{A}}$ radius of gyration in x
$\mathrm{r}_{\mathrm{y}}=\sqrt{\frac{\mathrm{I}_{\mathrm{y}}}{\mathrm{A}}}$ radius of gyration in y
$r_{o}=\sqrt{\frac{J_{o}}{A}}$ polar radius of gyration, and $\mathrm{r}_{\mathrm{o}}{ }^{2}=\mathrm{r}_{\mathrm{x}}{ }^{2}+\mathrm{r}_{\mathrm{y}}{ }^{2}$


## The Parallel-Axis Theorem

- The moment of inertia of an area with respect to any axis not through its centroid is equal to the moment of inertia of that area with respect to its own parallel centroidal axis plus the product of the area and the square of the distance between the two axes.

$$
\begin{aligned}
I & =\int y^{2} d A=\int\left(y^{\prime}-d\right)^{2} d A \\
& =\int y^{\prime 2} d A+2 d \int y^{\prime} d A+d^{2} \int d A
\end{aligned}
$$


but $\int y^{\prime} d A=0$, because the centroid is on this axis, resulting in:
$I_{x}=I_{c x}+A d_{y}{ }^{2} \quad$ (text notation) or $I_{x}=\bar{I}_{x}+A d_{y}{ }^{2}$
where $\mathrm{I}_{\mathrm{cx}}\left(\operatorname{or} \overline{\mathrm{I}}_{\mathrm{x}}\right)$ is the moment of inertia about the centroid of the area about an $x$ axis and $\mathrm{d}_{\mathrm{y}}$ is the y distance between the parallel axes

Similarly $\quad \begin{array}{ll}I_{y}=\bar{I}_{y}+A d_{x}^{2} & \text { Moment of inertia about a } y \text { axis } \\ J_{o}=\bar{J}_{c}+A d^{2} & \text { Polar moment of Inertia } \\ r_{o}^{2}=\bar{r}_{c}^{2}+d^{2} & \text { Polar radius of gyration } \\ r^{2}=\bar{r}^{2}+d^{2} & \text { Radius of gyration }\end{array}$

* I can be negative again if the area is negative (a hole or subtraction).
** If $\bar{I}$ is not given in a chart, but $\bar{x} \& \bar{y}$ are: YOU MUST CALCULATE $\bar{I}$ WITH $\bar{I}=I-A d^{2}$


## Composite Areas:

$I=\sum \bar{I}+\sum A d^{2} \quad$ where $\quad \overline{\mathrm{I}}$ is the moment of inertia about the centroid of the component area d is the distance from the centroid of the component area to the centroid of the composite area (ie. $\mathrm{d}_{\mathrm{y}}=\hat{y}-\bar{y}$ )

## Basic Steps

1. Draw a reference origin.
2. Divide the area into basic shapes
3. Label the basic shapes (components)
4. Draw a table with headers of

$$
\text { Component, Area, } \bar{x}, \bar{x} A, \bar{y}, \bar{y} A, \bar{I}_{x}, d_{y}, A d_{y}^{2}, \bar{I}_{y}, d_{x}, A d_{x}^{2}
$$

5. Fill in the table values needed to calculate $\hat{x}$ and $\hat{y}$ for the composite
6. Fill in the rest of the table values.
7. Sum the moment of inertia ( $\overline{\mathrm{I}}$ 's) and $\mathrm{Ad}^{2}$ columns and add together.

Geometric Properties of Areas

| Rectangle |  | $\begin{aligned} \bar{I}_{x^{\prime}} & =\frac{1}{12} b h^{3} \\ \bar{I}_{y^{\prime}} & =\frac{1}{12} b^{3} h \\ I_{x} & =\frac{1}{3} b h^{3} \\ I_{y} & =\frac{1}{3} b^{3} h \\ J_{C} & =\frac{1}{12} b h\left(b^{2}+h^{2}\right) \end{aligned}$ | $\begin{aligned} & \text { Area }=b h \\ & \bar{x}=b / 2 \\ & \bar{y}=h / 2 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \bar{I}_{x^{\prime}}=\frac{1}{31} b h^{3} \\ & I_{x}=\frac{1}{12} b h^{3} \\ & \bar{I}_{y^{\prime}}=\frac{1}{36} b^{3} h \end{aligned}$ | $\begin{aligned} & \text { Area }=b h / 2 \\ & \bar{x}=b / 3 \\ & \bar{y}=h / 3 \end{aligned}$ |
| Circle |  | $\begin{aligned} \bar{I}_{x} & =\bar{I}_{y}=\frac{1}{4} \pi r^{4} \\ J_{O} & =\frac{1}{2} \pi r^{4} \end{aligned}$ | $\begin{aligned} & \text { Area }=\pi r^{2}=\pi d^{2} / 4 \\ & \bar{x}=0 \\ & \bar{y}=0 \end{aligned}$ |
| Semicircle |  | $\begin{aligned} & \bar{I}_{x}=0.1098 r^{4} \\ & \bar{I}_{y}=\pi r^{4} / 8 \end{aligned}$ | $\begin{aligned} & \text { Area }=\pi r^{2} / 2=\pi d^{2} / 8 \\ & \bar{x}=0 \quad \bar{y}=4 r / 3 \pi \end{aligned}$ |
| Quarter circle |  | $\begin{aligned} & \bar{I}_{x}=0.0549 \mathrm{r}^{4} \\ & \bar{I}_{y}=0.0549 \mathrm{r}^{4} \end{aligned}$ | $\begin{aligned} & \text { Area }=\pi r^{2} / 4=\pi d^{2} / 16 \\ & \bar{x}=4 r / 3 \pi \\ & \bar{y}=4 r / 3 \pi \end{aligned}$ |
| Ellipse |  | $\begin{aligned} & \bar{I}_{x}=\frac{1}{4} \pi a b^{3} \\ & \bar{I}_{y}=\frac{1}{4} \pi a^{3} b \\ & J_{O}=\frac{1}{4} \pi a b\left(a^{2}+b^{2}\right) \end{aligned}$ | $\begin{aligned} & \text { Area }=\pi a b \\ & \bar{x}=0 \\ & \bar{y}=0 \end{aligned}$ |
| Semiparabolic area <br> Parabolic area |  | $\begin{aligned} & \bar{I}_{x}=16 \mathrm{ah}^{3} / 175 \\ & \bar{I}_{y}=4 \mathrm{a} 3 \mathrm{~h} / 15 \end{aligned}$ | $\begin{aligned} & \text { Area }=4 a h / 3 \\ & \bar{x}=0 \quad \bar{y}=3 h / 5 \end{aligned}$ |
| Parabolic spandrel |  | $\begin{aligned} & \bar{I}_{x}=37 \mathrm{ah}^{3} / 2100 \\ & \bar{I}_{y}=\mathrm{a}^{3 \mathrm{~h}} / 80 \end{aligned}$ | $\begin{aligned} & \text { Area }=a h / 3 \\ & \bar{x}=3 a / 4 \quad \bar{y}=3 h / 10 \end{aligned}$ |

Example 1 (pg 257)

Find the moments of inertia ( $\left.\hat{x}=3.05 ", \hat{y}=1.05^{\prime}\right)$.


| Component | $\begin{gathered} I_{x c} \\ \left(\text { in. }^{4}\right) \end{gathered}$ | $\begin{gathered} d_{y} \\ \text { (in.) } \end{gathered}$ | $\begin{aligned} & A d_{y_{y}}{ }^{2} \\ & \text { (in. }{ }^{4} \end{aligned}$ | $\begin{gathered} I_{y c} \\ \left(\text { in. }_{4}\right) \end{gathered}$ | $\begin{gathered} d_{x} \\ \text { (in.) } \end{gathered}$ | $\begin{aligned} & A d_{x}{ }^{2} \\ & \left(\text { (in. }{ }^{4}\right) \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\frac{(1)(4)^{3}}{12}=5.33$ | 0.95 | 3.61 | $\frac{(4)(1)^{3}}{12}=0.33$ | 2.55 | 26.01 |
|  | $\frac{(7)(1)^{3}}{12}=0.58$ | 0.55 | 2.12 | $\frac{(1)(7)^{3}}{12}=28.58$ | 1.45 | 14.72 |
|  | $\sum I_{x c}=5.91$ |  | $\sum A d_{y}{ }^{2}=5.73$ | $\sum I_{y c}=28.91$ |  | $\sum A d_{x}=40.73$ |

Example 2 (pg 253)
Example Problem 7.6 (Figures 7.24 to 7.26 )
Determine the $I$ about the centroidal $x$-axis.


## Example 3

Determine the moments of inertia about the centroid of the shape.

Solution:
There is no reference origin suggested in figure (a), so the bottom left corner is good.

In figure (b) area A will be a complete rectangle,

(a)

(b) while areas $C$ and $A$ are "holes" with negative area and negative moment of inertias.

| Area $A=200 \mathrm{~mm} \times 100 \mathrm{~mm}=20000 \mathrm{~mm}^{2}$ | $\mathrm{I}_{\mathrm{x}}=(200 \mathrm{~mm})(100 \mathrm{~mm})^{3} / 12=16.667 \times 10^{6} \mathrm{~mm}^{4}$ <br> $\mathrm{I}_{\mathrm{y}}=(200 \mathrm{~mm})^{3}(100 \mathrm{~mm}) / 12=66.667 \times 10^{6} \mathrm{~mm}^{4}$ |
| :--- | :--- |
| Area $B=-\pi(30 \mathrm{~mm})^{2}=-2827.4 \mathrm{~mm}^{2}$ | $\mathrm{I}_{\mathrm{x}}=\mathrm{I}_{\mathrm{y}}=-\pi(30 \mathrm{~mm})^{4} / 4=-0.636 \times 10^{6} \mathrm{~mm}^{4}$ |
| Area $C=-1 / 2 \pi(50 \mathrm{~mm})^{2}=3927.0 \mathrm{~mm}^{2}$ | $\mathrm{I}_{\mathrm{x}}=-\pi(50 \mathrm{~mm})^{4 / 8=-2.454 \times 10^{6} \mathrm{~mm}^{4}}$ |
| Area $D=100 \mathrm{~mm} \times 200 \mathrm{~mm} \times 1 / 2=10000 \mathrm{~mm}^{2}=-0.1098(50 \mathrm{~mm})^{4}=-0.686 \times 10^{6} \mathrm{~mm}^{4}$ |  |
|  | $\mathrm{I}_{\mathrm{x}}=(200 \mathrm{~mm})(100 \mathrm{~mm})^{3} / 36=5.556 \times 10^{6} \mathrm{~mm}^{4}$ <br> $\mathrm{I}_{\mathrm{y}}=(200 \mathrm{~mm})^{3}(100 \mathrm{~mm}) / 36=22.222 \times 10^{6} \mathrm{~mm}^{4}$ |


| shape | $A\left(\mathrm{~mm}^{2}\right)$ | $\overline{\mathrm{X}}(\mathrm{mm})$ | $\overline{\mathrm{X}} \mathrm{A}\left(\mathrm{mm}^{3}\right)$ | $\overline{\mathrm{y}}(\mathrm{mm})$ | $\overline{\mathrm{y}} \mathrm{A}\left(\mathrm{mm}^{3}\right)$ |  |
| :--- | ---: | ---: | ---: | ---: | :--- | :--- |
| A | 20000 | 100 | 2000000 | 50 | 1000000 | $\hat{x}=\frac{2159218 \mathrm{~mm}^{3}}{23245.58 \mathrm{~mm}^{2}}=92.9 \mathrm{~mm}$ |
| B | -2827.43 | 150 | -424115 | 50 | -141372 |  |
| C | -3926.99 | 21.22066 | -83333.3 | 50 | -196350 | $\hat{y}=\frac{1995612 \mathrm{~mm}^{3}}{23245.58 \mathrm{~mm}^{2}}=85.8 \mathrm{~mm}$ |
| D | 10000 | 66.66667 | 666666.7 | 133.3333 | 1333333 |  |
|  |  | 2159218 |  | 1995612 |  |  |


| shape | $\mathrm{I}_{\mathrm{x}}\left(\mathrm{mm}^{4}\right)$ | $\mathrm{d}_{\mathrm{y}}(\mathrm{mm})$ | $\mathrm{Ad}_{\mathrm{y}}{ }^{2}\left(\mathrm{~mm}{ }^{4}\right)$ | $\mathrm{I}_{\mathrm{y}}\left(\mathrm{mm}^{4}\right)$ | $\mathrm{d}_{\mathrm{x}}(\mathrm{mm})$ | $\operatorname{Ad}_{x}{ }^{2}\left(\mathrm{~mm}{ }^{4}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A | 16666667 | 35.8 | 25632800 | 66666667 | -7.1 | 1008200 |
| B | -636173 | 35.8 | -3623751.73 | -636173 | -57.1 | -9218592.093 |
| C | -2454369 | 35.8 | -5032988.51 | -686250 | 71.67934 | -20176595.22 |
| D | 5555556 | $-47.5333$ | 22594177.8 | 2222222 | 26.23333 | 6881876.029 |
|  | 19131680 |  | 39570237.5 | 87566466 |  | -21505111.29 |

So, $\quad \mathrm{I}_{\mathrm{x}}=19131680+39570237.5=58701918=58.7 \times 10^{6} \mathrm{~mm}^{4}$
$I_{x}=87566466+-21505111.3=43572025=66.1 \times 10^{6} \mathrm{~mm}^{4}$

Example 4 (pg 258)
Example Problem 7.10 (Figures 7.35 and 7.36)
Locate the centroidal $x$ and $y$ axes for the cross-section shown. Use the reference origin indicated and assume that the steel plate is centered over the flange of the wide-flange section. Compute the $I_{x}$ and $I_{y}$ about the major centroidal axes.


Example 5 (pg 249)*
Example Problem 7.5 (Figures 7.16 and 7.17)
A composite or built-up cross-section for a beam is fabricated using two $1 / 2^{\prime \prime} \times 10^{\prime \prime}$ vertical plates with a $\mathrm{C} 12 \times 20.7$ channel section welded to the top and a W12 $\times 16$ section welded to the bottom as shown. Determine the location of the major $x$-axis using the center of the W12 $\times 16$ 's web as the reference origin. Also determine the moment of inertia about both major centroidal axes.


| shape | $1_{x}\left(\mathrm{in}^{4}\right)$ | $\mathrm{d}_{\mathrm{y}}$ (in) | $\mathrm{Ad}_{\mathrm{y}}{ }^{2}\left(\mathrm{in}^{4}\right)$ | $\mathrm{I}_{\mathrm{y}}\left(\mathrm{in}^{4}\right)$ | $\mathrm{d}_{\mathrm{x}}$ (in) | $A d_{x}{ }^{2}\left(\mathrm{in}^{4}\right)$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| channel | 3.880 | -4.399 | 117.849 | 129.000 | 0.000 | 0.000 |
| left plate | 41.667 | 0.185 | 0.171 | 0.104 | 3.250 | 52.813 |
| right plate | 41.667 | 0.185 | 0.171 | 0.104 | -3.250 | 52.813 |
| wide flange | 2.800 | 5.295 | 132.054 | 103.000 | 0.000 | 0.000 |
|  | 90.013 |  | 250.245 | 232.208 |  | 105.625 |

$I_{x}=90.013+250.245=340.259=340.3 \mathrm{in}^{4}$
$I_{y}=232.208+105.625=337.833=337.8$ in $^{4}$

